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BY PREDERICK T. SIMON
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UNITED STATES ARMY NATION EARCH & DEVELOPMENT LABORATORIES NATION, MASSACHUSETTS 07760

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20. ABSTRACT (Continue on reverse of the reservery and identity by block number) developed to check that a color measuring instrument and that measurements made with it are within accept	will perform satisfactorily
of materials were selected to test the instrument: a	white opal tile to check
nominal 100% reflectance; an amber glass filter to c	heck low and high photo-
metric scale and the wavelength scale at mid range;	a gray porcelain tile to
check the reflectance scale at mid range; and a pair to check that proper color differences are being mea	sured and calculated. Two
instruments were used in this study, a Hunterlab D54	spectrophotometer and a

Unclassified SECURITY CLASSIFICATION OF THIS PAGE(When Date Entered) 20. Diano Match-Scan spectrophotometer. Each was interfaced to a mini-computer for collecting data on the test materials. Based on statistical studies of the measurements made on the instruments, two slightly different computer programs were developed which provide guidance for the operator of the instrument through the standardization procedure and make comparisons of the current measured data to previously established norms and tolerances for the same material. The computer programs are "fail-safe" in the sense that the instrument cannot be used to perform routine tests unless all of the standardization criteria are met.

PREFACE

The work reported was performed as part of Phase II of a project to develop a color measuring system to be used for instrument judgment of color of textile fabrics procured by the Defense Department. The heart of the system is a spectrophotometer to be controlled by a computer that also performs required colorimetric calculations.

Phase I was limited to an evaluation of commercially available spectrophotometers, each with a small microprocessor. The evaluation was performed under Contract DAAK60-77-C-0093 by Rensselaer Polytechnic Institute and published as NATICK/TR-79/044. All three instruments evaluated were judged capable of meeting the color requirements. Because the system also must be capable of measuring infrared reflectance, however, one of the three instruments was dropped from further consideration in the system development.

The purpose of Phase II was to design the color measurement system to meet the needs of the program. One step in the design was the development of a mathematical means for expressing acceptability of slight deviations from standard shade. This work was performed under Contract DAAK60-78-C-0084 by Lehigh University and published as NATICK/TR-80-0036. A second step was development of a rigid system calibration procedure, which is the subject of this report. The work was performed under Contract DAAK60-79-C-0096 by Clemson University. The third step under Phase II was design and procurement of a prototype, two-unit system.

Support of the program was provided by the Manufacturing Testing Technology program. The Project Officer throughout both Phase I and Phase II was Alvin O. Ramsley; Alternate Project Officer was Therese R. Commerford.

The project officers acknowledge with thanks the constructive suggestions made by the Committee on Color Measurement of the National Research Council. Committee members are David L. MacAdam, Chairman, Ellen C. Carter, Franc Grum, Robert F. Hoban, Michael E. Breton and John J. Hanlon.

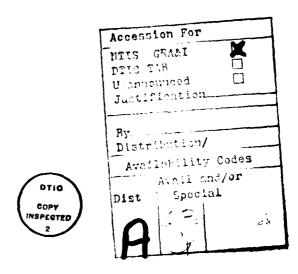


TABLE OF CONTENTS

	Page
Preface	1
List of Figures	4
List of Tables	4
Introduction	5
Instrumentation Used In Study	5
Basic Calibration Methods	6
Routine Calibration	8
Working Calibration Method	10
Observations	11
Bibliography	12
Appendix A: Computer Program QMSTAT for Match-Scan Star Study.	tistical 41
Appendix B: Computer Program QMSTAT for Hunter D54 Sta Study.	tistical 45
Appendix C: Computer Program QMSTAN for Standardization Match-Scan.	n Program of 49
Appendix D: Computer Program QSTANH for Standardization Hunter D54.	n Program of 53

ILLUSTRATIVE DATA

		Page
Figure 1. Transm Match-Scan instru	mission curve of didymium filter for Hunter and ments.	16
Figure 2. Match-	Scan wavelength calibrating filters.	17
Figure 3. Hunter	wavelength calibrating filters.	18
Figure 4. Mercur	y emission lines on the Match-Scan instrument.	19
Figure 5. Reflect Match-Scan.	ctance of opal and gray porcelain tiles with	20
Figure 6. Reflection Hunter D54.	ctance of opal and gray porcelain tiles with	21
Figure 7. Transm	nittance of amber filter with Match-Scan.	22
Figure 8. Transm	nittance of amber filter with Hunter D54.	23
Figure 9. Reflect Match-Scan.	tance curves of a pair of tan specimens with the	24
Figure 10. Reflection Hunter D54.	ctance curves of a pair of tan specimens with the	25
Figure 11. Statis	tical study for Match-Scan.	26
Figure 12. Statis	stical study for Hunter D54.	30
Figure 13. Schema	atic of standardization of Match-Scan.	34
Figure 14. Schema	atic of standardization of Hunter D54.	35
Figure 15. Standa QMSTAN computer p	ardization test for Match-Scan, typical output from program.	36
Figure 16. Standa QSTANH computer p	ardization test for Hunter D54, typical output from program.	37
	ission data on NG-9 and NG-3 neutral gray filters tional Bureau of Standards at 511 nm, measurements	13
	ission data on NG-4 and NG-5 neutral gray filters ional Bureau of Standards at 511 nm, measurements	14
Table 3. Measure	ed values for calibration materials.	15

Introduction

The U.S. Army Natick Research and Development Laboratories entered into a contract with Clemson University to have a method developed for the standardization of color measuring instruments. This is one part of the longer range program to evolve an inspection procedure for the acceptance of the color of military fabrics through instrumental measurement rather than by visual estimation. Although there are several problems to be solved before a reliable procedure is achieved, two of the major aspects of the project have been investigated under contract and reported separately. In one of these contracts Billmeyer and Alessi addressed the general reliability of commercial color instruments, and in the other one Allen and Yuhas developed the mathematics of the color acceptability criteria. The present work covers a third aspect which involves the technique that would be used to assure reliability of the instrumental measurement through proper calibration.

Instrumentation used in study

Two instruments were used to develop and test the standardization procedure. Both instruments are commercially available and had been investigated in an earlier contract and had been found in the main to be suitable. One instrument is the Hunter D54 spectrophotometer (Christie and McConnell, 1977) and the other is the Diano Match-Scan spectrophotometer. Except for the fact that both instruments involve integrating spheres and diffuse polychromatic illumination, the optical arrangement of the two is quite different. Nevertheless, the measurement data obtained in this study with both instruments were quite comparable although they were not exactly interchangeable. No attempts were made to introduce adjustments to compensate for these small differences in results.

The Hunter spectrophotometer was loaned to Clemson by Natick Laboratories for the purpose of this study. It consisted of three interconnected units: a measuring head, power supply, and a microprocessor push-button controller. In order to collect the large amount of statistical data required in this work, the instrument controller was interfaced to a General Automation SPC-16/45 minicomputer. On occasions when graphical data were needed, the spectrophotometer was connected to a Tektronik 4662 plotter. The SPC-16 was programmed in Fortran to aid in the data collection and the standardization test procedure.

^{1.} F. W. Billmeyer, Jr. and P. J. Alessi (1979, "Assessment of Color-Measuring Instruments for Objective Textile Acceptability Judgement" Technical Report NATICK/TR-79/044, U.S. Natick Research and Development Command, Natick, MA 01760, March 1979.

^{2.} E. Allen, and B. Yuhas (1980), "Investigations to Define Acceptability Tolerance Ranges in Various Regions of Color Space," Technical Report, NATICK/TR-80/036, U.S. Army Natick Research and Development Command, Natick, MA 01760, September 1980.

J. S. Christie, and G. McConnell, Color 77, p. 309, Adam Hilger Ltd., Bristol, England, 1977.

The Diano Match-Scan spectrophotometer is part of an integrated instrument computer system called the Match-Mate 3000. The instrument is entirely computer-controlled which means that special test programs were written in Fortran around operating software that was furnished by the manufacturer. The Tektronik 4662 plotter was also interfaced to the Match-Mate 3000 system for drawing special graphs.

Basic calibration methods

Spectrophotometric reflectance data are the basic measurements used for calculating color difference values which in turn express the acceptability of the color of test materials compared to established standards. Therefore, it is necessary to evolve a method that would establish with a fair degree of certainty that the instrumental measurement is reliable in order that a high degree of confidence can be placed on tests performed with the equipment. Such a premise infers that the instrument is set up for operation and then checked according to prescribed methods. It must be relative to some accurately known set of data. If these data are based on fundamental measurement of wavelength and spectral power, then this is an absolute method. Alternatively, the values of a set of calibrating materials can be known relative to a master set of similar materials; when the instrument is performing satisfactorily, the results obtained on a specific set of materials will be within specified tolerances. This is a relative calibration method. In this application, long term repeatability of measurements of a given instrument and reproducibility of measurements between locations are of paramount importance, therefore, the relative calibration method is followed in the present study.

Wavelength scale calibration has been done for many years on several commercial spectrophotometers using the well-known absorption maximum of the Corning 5120 didymium glass. Gibson, and Keegan found that several maxima can be used with spectrophotometers having a constant bandwidth in the range between 2 and 10 nm; this offers a method for checking spectrophotometers that have such resolution. Although the Match-Scan can be calibrated with didymium, this procedure is inappropriate for the D54 instrument which has a bandwidth that changes from 12 nm at 400 nm to 18 nm to 700 nm, making the didymium filter less suited to this purpose. This is shown in Figure 1. Venable and Eckerele (1979) have described a more advanced method for wavelength calibration with a didymium filter which is suitable for any wavelength bandpass.

^{4.} K. S. Gibson, and H. J. Keegan, J. Opt. Soc. Am. 31, 462 (1941).

^{5.} W.TH. Venable, Jr., and K. L. Eckerle, (1979), "Didymium Glass Filters for Calibrating Wavelength Scale of Spectrophotometer-SRM 2009, 2010, 2013 and 2014," NBS Special Publication 260-66. National Bureau of Standards, Washington, DC 20234.

An alternative method for wavelength calibration was described by 7 Van den Akker and adapted for the D54 instrument by Stanziola et al. It requires pairs of glass filters having spectrophotometric curves that cross at a determinable wavelength. In the region of the crossing, it is best that the transmission curves be approximately linear. Two sets of filters have been used to check the wavelength scales around 440 nm and 590 nm which presumes to cover the limits of the visible spectrum. The Van den Akker method is applicable to both the D54 and Match-Scan; curves obtained with each instrument are shown in Figures 2 and 3.

There are caveats to the crossing-filter method. Individual sets of filters give particular wavelength crossings which are dependent as well upon bandwidth and instrument geometry. Different values for the intersection wavelength will also be obtained depending upon what wavelength increment is used to interpolate among the transmission measurements for each pair of filters. The crossing wavelength can be computed with data from any wavelength interval according to the following formula:

$$X = I(t_3-t_1)/(t_2+t_3-t_1-t_4) + W$$

where,

X is the crossing wavelength

I is the wavelength increment

 t_1 , t_2 are the transmittances for the first filter at wavelength, W, and wavelength, W + I, respectively

 $\mathsf{t_{3}},\;\mathsf{t_{4}}$ are the transmittances for the second filter at the same wavelengths as the first filter

W is the first wavelength

A 10-nm increment is preferred because it is a normal mode of operation for the D54 instrument and this makes for a convenient procedure. Hunterlab makes their determinations at 1-nm intervals, which give slightly more variable data (see below) than with 10-nm intervals. There is a small difference in the crossing wavelength dependent upon the wavelength increment, but as long as the same procedure is used at all times, the resulting values should be consistent.

Another method based on mercury emission lines is suited to the Match-Scan instrument but not the D54. The Match-Scan is provided with a Stand-Alone

^{6.} J. A. Van den Akker, J. Opt. Soc. Am. 33, 257 (1943).

^{7.} R. Stanziola, B. Momiroff, and H. Hemmendinger, Color Research Application 4, 36 (1979).

Program (SAP) which allows for single-beam radiometric measurements at 0.2-nm intervals. The output of a mercury arc lamp can be scanned around the emission peaks at 404.7, 435.7, 546.1, 557-578 to determine whether the instrument wavelength scale is correct. This has been done with the Match-Scan and the results are shown in Figure 4. Although the instrument has not been reset to the correct wavelength, the wavelength error is repeatable over a six-month period indicating that reproducible measurements can be achieved.

The D54 is routinely calibrated by the manufacturer, Hunterlab, using a series of filters of known spectral transmittance values for corresponding wavelengths. Diano, on the other hand, calibrates the Match-Scan using the didymium filter absorption points. However, the purpose of this procedure is to recognize whether an instrument is performing in the same way that it had been when it was put into service. To that end a simple wavelength check is made with the transmittance of an anber filter at about the middle of the visible spectral range.

Several methods have been cited for wavelength checking but there are not generally accepted methods for establishing the validity of the photometric (reflectance or transmittance) scale for a spectrophotometer. In cooperation with the National Bureau of Standards we have developed a set of four neutral gray glass filters of ascending transmittances from about 0.5% to 31%. These were measured on the NBS high-accuracy spectrophotometer at 511 nm, which is in an area of relatively flat transmittance. Since the high-accuracy spectrophotometer will give transmittance values at least more precise than any commercial instrument, it was felt that these filters would serve as a good reference for both instruments in this study.

The measurements obtained on the instruments are given in Tables 1 and 2. It will be noted that 1-nm data obtained with the D54 are slightly less consistent than data obtained with the Match-Scan. For reasons not known, these data are not in keeping with the 10-nm data obtained on the D54 in other parts of this study. Although the photometric readings on both instruments are not equal to those of the NBS, repeat tests done weeks apart indicate that the departure from the Bureau's values remains constant. One can presume from this that either the method of measurement in the commercial instruments produces a specific bias or that the normal standardization methods for these instruments do not compensate for nonlinearity in the photometric scale. Nonetheless, consistency of results is the overwhelming requirement.

Routine calibration

The calibration method which was finally developed as a result of this investigation considered that the following criteria were important:

a. Physical samples should be measured on the instrument and should be stable, easily cleaned, and of a convenient size.

^{8.} See Reference 3.

^{9.} See Reference 5.

- b. Measurements should check the performance or the instrument as for wavelength reliability as well as low range (below 5%) and high range (above 70%) photometric response.
- c. Measurements should also check the 100% line and the mid-scale correction in the reflection mode.
- d. A final check should be made of the ability of the instrument and computer system to give reproducible color difference values on a pair of samples of known color difference.
- e. Backup calibration materials should be available to check the instrument wavelength if there are indications of wavelength uncertainty in the routine test.

These objectives were satisfied by selection of the following materials:

- a. A white opal glass, 50 mm square by 10 mm thick which is covered on back and sides with black paper. See Figures 5 and 6.
- b. A Corning 3307 Signal Yellow filter, 50 mm square by 2.3 thick. See Figures 7 and 8.
- c. A gray porcelain enamel plaque, 10.7 cm square. See Figures 5 and 6.
- d. A pair of tan polyester gelcoat plaques, 7.8 mm square. See Figures 9 and 10.
- e. Four glass filters for wavelength checking. Each is 50 mm square. These filters were obtained through Hunter Associates Laboratory (the Corning description is only given for reference).

Blue-Corning 5851, 2.8 mm thick Green-Corning 4445, 5.0 mm thick Yellow-Corning 3387, 3.0 mm thick Red-Corning 2424, 3.1 mm thick

Six sets of these calibration materials were obtained and checked for similarity. Only one set of materials was used throughout this study; individual values for the remaining five sets are given in Table 3 of this report.

In order to establish the range of expected values that would be obtained when the calibrating materials are measured on each instrument, two Fortran programs were written to assist in the collection and evaluation of the resulting data. The programs are the same in principle, but since each instrument operates differently and is interfaced to its own computer, small changes were made to fit each case. QMSTAT is the program used with the Diano Match-Scan and its Digital Equipment Company LSI-11 computer and QMSTA1 is used with the Hunter D54 spectrophotometer and the General Automation SPC-16 computer.

The procedure used for the calibration samples with the Match-Scan, made it simple to measure the samples in sequence:

Opal glass Amber filter Gray porcelain enamel tile Standard tan plastic Sample tan plastic

Each sample was carefully washed with a 1% solution of Sparkleen (Fisher Scientific Company), rinsed with distilled water and carefully dried with Kimwipes. This was done before every measurement.

In the case of the D54 instrument, a procedure that includes instrument setup was added:

Set up D54 for transmittance:

- a. Press "TRANS" button
- b. Block beam with black cardboard and press "ZERO"
- c. Insert white tile and press "STDZ"

Measure Amber filter

Set up D54 for reflectance:

- a. Press "R-SIN" button
- b. Place black trap over port and press "ZERO"
- c. Place white tile over port and press "STDZ"
- d. Place gray tile over port and press "STDZ"

Measure Opal glass Measure Gray porcelain enamel tile Measure Standard tan plastic Measure Sample tan plastic

Both QUMSTAT and QMSTAl programs provide the necessary prompting so that the operator follows the proper sequence. In the QMSTAT program the paired white opal glasses are assumed to be approximately matched, and all of the subsquest measures are corrected to a value which compensates for any mismatch. A set of measurements and calculations for both instruments are given as Figures 11 and 12. Note that all spectral data lists the results of a single measurement, the average of two measurements and the average of ten measurements. Based on these data and the calculated standard deviation (sigma), it was concluded that the average of two measurements was suitable. Since we were not able to actuate the D54 through the program on the SPC-16 computer, we were obliged to operate the spectrophotometer through the keyboard and collect the resulting data through and ASCII interface to the computer. This was accomplished by first pressing the "READ" button; then when the "BUSY" light went out, the "10 NM" button on spectrophotometer console and the "RETURN" on the computer keyboard were pressed simultaneously.

A "PAUSE" was built into the computer program to allow for these operations to take place. Figure 12 shows that the ten repeat measurements were made with a PAUSE between each set. Analogous data to those shown for the Match-Scan in Figure 11 were obtained for the D54 instrument. In preparing Figure 12, the intermediate PAUSE statements have not been shown.

Working Calibration Method

The statistical studies with the two instruments were carried on for several months to establish a long term record of performance with the calibrating materials. Based on these experiments, two new programs QMSTAN for the Match-Scan and QMSTANH for the D54 were written to serve as a "fail-safe" calibration procedure that will not permit operation of the instrument if it fails within the limits set for each material. Again there are some differences between the instruments in the procedure itself as well as the specific limits set for each material. Figures 13 and 14 give a diagram of the information needed to effect the calibration of each instrument. Figure 15 shows a set of data obtained with the Match-Scan and Figure 16 shows a set of data obtained with the D54 spectrophotometer.

Observations

Table 3 summarizes the values obtained with each set of materials that are recommended for standardization of any spectrophotometer similar to the D54 or Match-Scan. The tolerances given in the Table reflect the experience obtained from this study. In the main, the tolerance that were determined for acceptable instrument performance in the QMSTAN and QSTANH programs are similar, since both instruments performed in a comparable manner. The data that were obtained on Set #1 were specifically determined on both instruments at $76^{\circ} + 1^{\circ}$ F. All of the other data were obtained on the Match-Scan.

Slightly larger tolerances are given for the D54 than the Match-Scan, which allows for the change in transmittance when the D54 is operated at 84°F. Experiments were repeated twice with the temperature in the Clemson Color Science Center laboratory raised to 84°F. When this was done, the transmittance of the amber filter as measured by the D54 was slightly lower than typical results obtained at 76°F. The measurements performed on the Match-Scan at the same time did not show any difference between the two temperatures. If one can assume that the transmittance of the amber filter is approximately linear between 520 and 530 nm, 1% change in transmittance is equivalent to a 0.63 nm wavelength change. Therefore, the tolerance of 0.3% is equivalent to about 0.19 nm for the D54 and 0.13 for the Match-Scan. No statistically significant color differences were determined for the twn plastic samples when the data obtained at 76°F were compared to those at 84°F.

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Table 1. Transmission Data on NG-9 and NG-3 Neutral Gray Filters Calibrated by National Bureau of Standards at 511 nm; measurements at 1-nm intervals.

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516.0				513	.81
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519.0				515	.83
519.0	0.82			516	.84
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SAMPLE				520	. 82
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NG-3 AVERAI NO. OI Nat W/L 505.0 507.0 509.0 510.0 512.0 513.0 514.0 515.0	NBS Value GE READINGS 7 F READINGS TO chscan ZR 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74	EN/NJ Y		TRANSM 505 506 507 508 509 510 511 512 513	D 54 D 54 D 54 D 57 D 57 D 58
NG-3 AVERAI NO. OI Nat W/L 505.0 507.0 509.0 510.0 512.0 513.0 514.0 515.0	NBS Value DE READINGS 7 F READINGS TO chscan 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74	EN/NJ Y		TRANSM 505 506 507 509 510 511 512 513 514 515	D 54 D 54 D 54 D 57 D 57 D 58
NG-3 AVERAI NO. OI Mat W/L 505.0 507.0 508.0 519.0 511.0 511.0 515.0 516.0 517.0	NBS Value SE READINGS 7 F READINGS TO chscan 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74	EN/NJ Y		TRANSM 505 506 507 508 510 511 512 513 514 515	D 54 D 54 D 54 D 54 D 54 D 54 D 54 D 54
NG-3 AVERAI NO. OI Mat W/L 505.0 507.0 508.0 510.0 512.0 513.0 514.0 515.0 516.0	NBS Value SE READINGS 7 F READINGS TO chscan 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74	EN/NJ Y		TRANSM 505 506 507 508 509 510 511 512 513 514 515 516 517	D 54 NITTANCE 2.74 2.77 2.72 2.73 2.73 2.75 2.74 2.74 2.74 2.76 2.78 2.75
NG-3 AVERAG NO. OF Mat W/L 505.0 507.0 509.0 510.0 512.0 514.0 515.0 516.0 517.0	NBS Value SE READINGS 7 F READINGS TO chscan 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.7	EN/NJ Y		TRANSM 505 506 507 508 509 510 511 512 513 514 515 516 516 517	D 54 IITTANCE 2.74 2.77 2.76 2.73 2.75 2.74 2.74 2.76 2.78 2.75 2.77
NG-3 AVERAG NO. OF Mat W/L 505.0 507.0 509.0 510.0 512.0 512.0 512.0 512.0 512.0 512.0	NBS Value SE READINGS 7 F READINGS TO chscan 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74 2.74	EN/NJ Y		TRANSM 505 506 507 508 509 510 511 512 513 514 515 516 517	D 54 NITTANCE 2.74 2.77 2.72 2.73 2.73 2.75 2.74 2.74 2.74 2.76 2.78 2.75

Table 2. Transmission Data on NG-4 and NG-5 Neutral Gray Filters Calibrated by National Bureau of Standards at 511 nm; Measurements at 1-nm intervals.

SAMPLE RAME?		
NG-4 NBS Value 4.384		
AVERNOE REALINGS ? LYZN Y		
NO. OF READINGS TO AVERAGE? 2	D !	54
Matchscan		, 4
W/L %K	TRANSM17	CTANCE
505.0 4.49	TRANSIT	IMIYUE
506.0 4.48	p , p	
507.0 4.48	505	4.51
500.0 4.47	506	4.52
	597	4.44
509.0 4.48	508	4.50
510.0 4.47	509	4.49
511.0 4.47	510	4.48
512.0 4.47	511	4.50
513.0 4.47	512	4.47
514.0 4.47	513	
515.0 4.49		4.49
516.0 4.49	514	4.49
517.0 4.50	515	4.47
518.0 4.51	516	4.54
519.0 4.52	517	4.53
520.0 4.53	518	4.47
CONTINUE? CYNNI Y	519	4.51
	520	4.48
SAMPLE NAME?	020	7,70
NG-5 NBS Value 31.145%		
AVERAGE READINGS ? [Y/N] Y	D 5	A
NO. OF READINGS TO AVERAGE? 2	., .	7
Matchscan	TRANSMIT	TONCE
W/L %F:	INMINORITI	IMITOL
505.0 31.47	FOE	74 50
506.0 31.47	505	31.59
507.0 31.47	506	31.61
508.0 31.45	597	31.61
509.0 31.48	508	31.65
510.0 31.46	509	31.62
	510	31.65
511.0 31.47	511	31.70
512.0 31.46	512	31.69
513.0 31.47	513	31.64
514.0 31.48		
515.0 31.50	514 E15	31.67
516.0 31.51	515 516	31.63
517.0 31.53	516	31.69
518.0 31.55	517	31.59
519.0 31.55	518	31. <i>6</i> 9
520.0 31.61	519.	31.62
CONTINUET LYNNT Y	528	31.66

Table 3. Measured Values for Calibration Materials.

				Set Number 1	er 1	1	Mea	n T or R	in % -	Mean T or R in % - other sets	ţ.
		Match-scan	scan	Ο,	D54	#5	#3	#	# 2	9#	
	Mean Length	Mean T or R	Tolerance	Mean T or R	Tolerance						
White Tile	540	100.02*	⁺ 0.07	98.36	-0.10	100.08	100.17	96.66	100.03	96.66	9-6
Amber Filter	420	3.50	⁺ 0.03	3.48	[‡] 0.03	3.81	3.57	3.39	3.02	2.54	3-2
	520	39.15	[‡] 0.12	38.68	- 0.18	40.21	39.36	38.96	37.66	35.86	3-6
	099	79.97	1 0.12	80.20	[‡] 0.12	80.06	79.81	79.61	79.19	78.43	> 4
Gray Porcelain Tile	540	43.90	1 0.10	42.96	÷0.10	44.66	44.57	43.96	44.33	45.03	> 4
Tan Plastic -		Mean	Tolerance	Mean	Tolerance	Mean	Mean	Mean	Mean	Mean	
CIEL* a* b* 1976		1.89	±0.05	1.88	-0.05	2.06	1.98	1.97	2.10	1.90	Delta E
	Wave Length										
Filter Pair											
Ok Blue - Yellow	441.3					441.3	438.9	441.3	440.4	442.2	æ
Red-Blue Green	590.1					590.1	589.3	590.1	591.0	589.6	٤

15

*Sample versus Standard tile

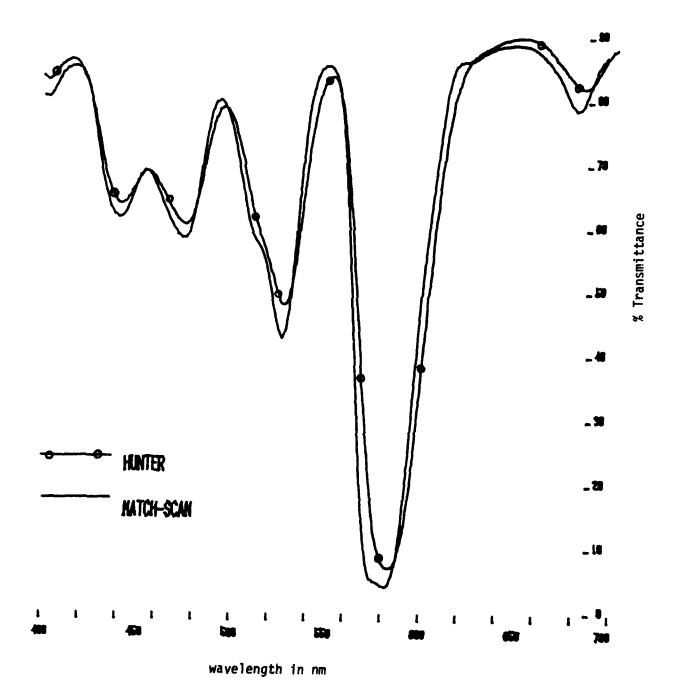


Figure 1. Transmission curves of didymium filter for Hunter D54 and Match-Scan instruments.

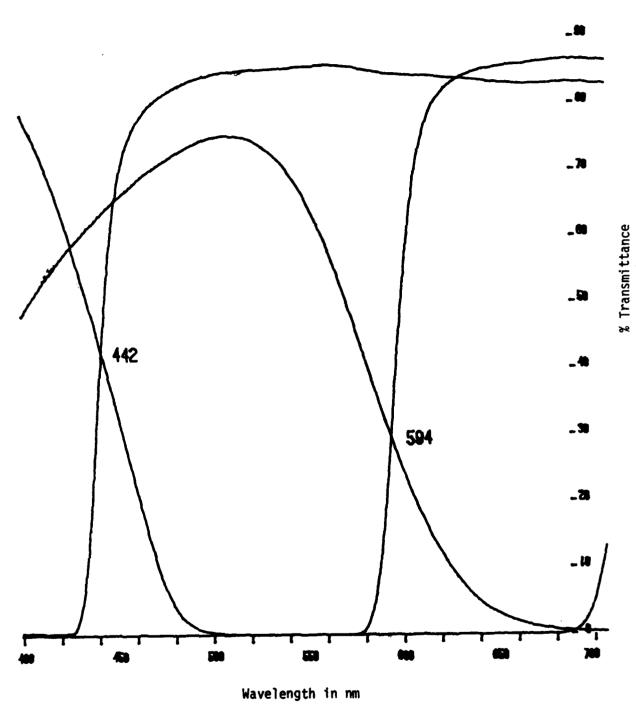


Figure 2. Match-Scan wavelength calibrating filter transmission curves.

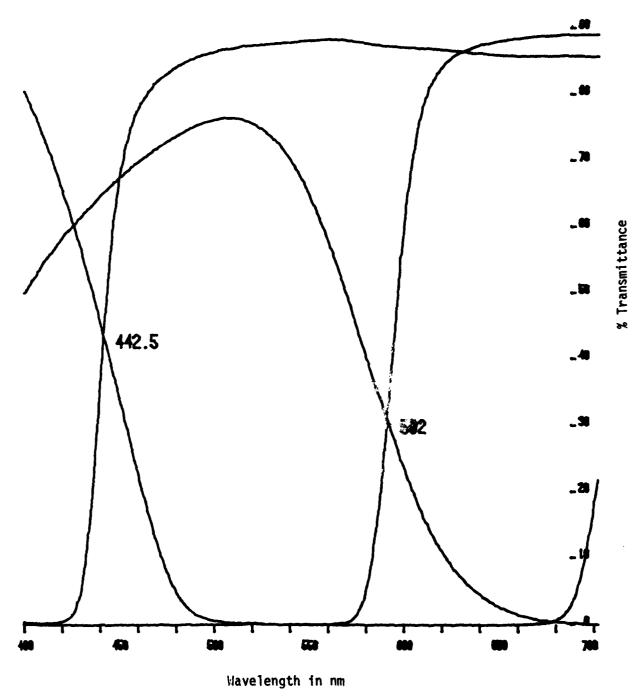


Figure 3. Hunter D54 wavelength calibrating filter transmission curves.

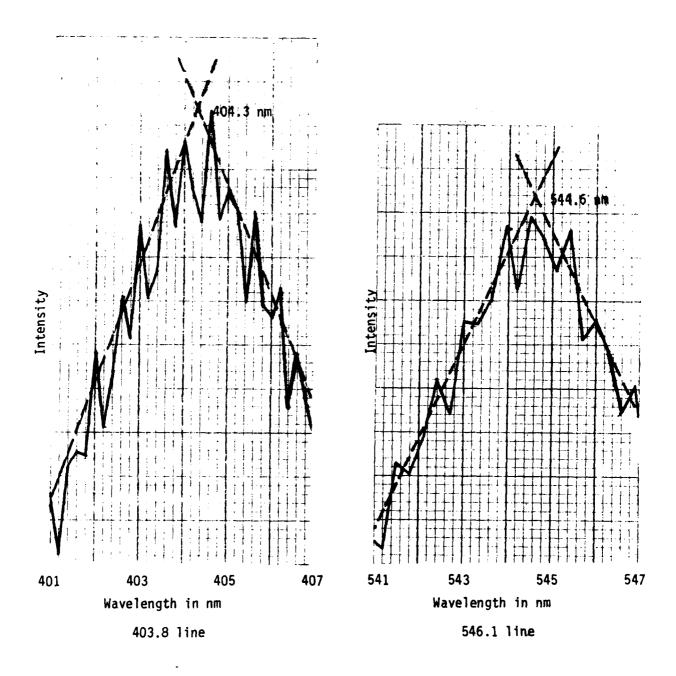


Figure 4. Mercury emission lines on the Match-Scan instrument.

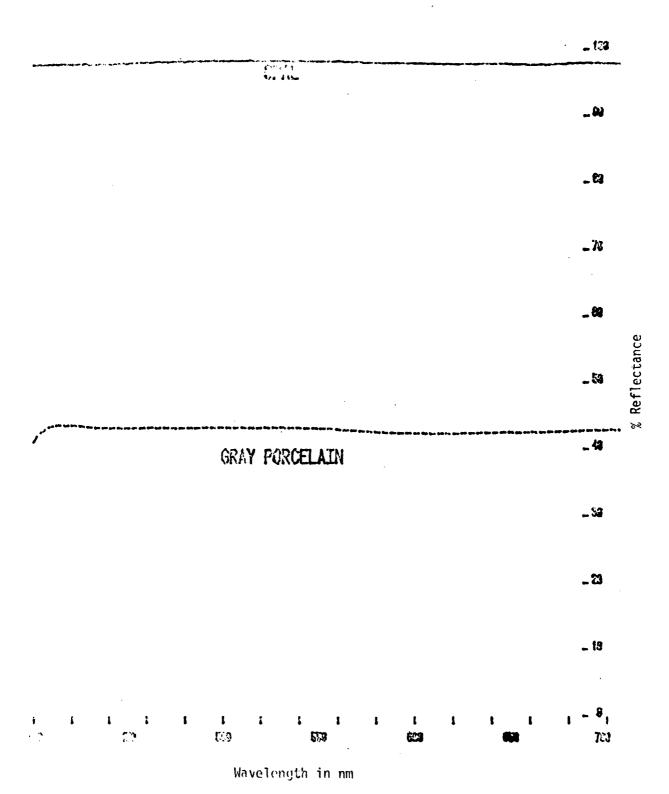


Figure 5. Reflectance of opal and gray porcelain tiles with Match-Scan.

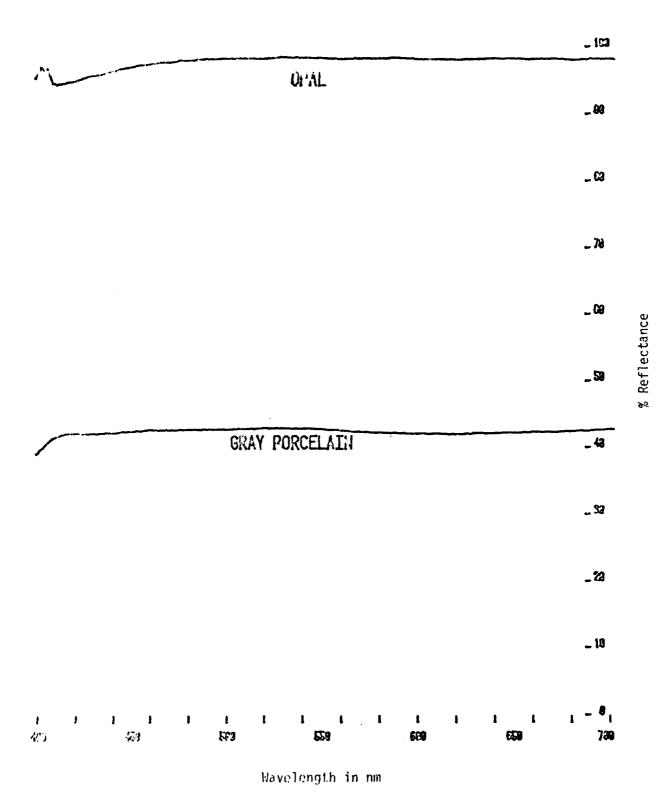


Figure 6. Reflectance of opal and gray porcelain tiles with Hunter D54.



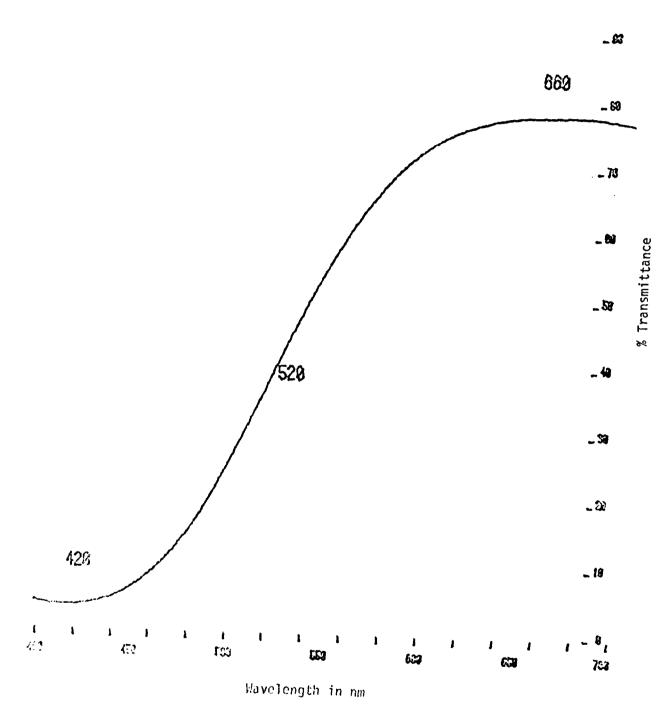


Figure 7. Transmittance of amber filter with Match-Scan.

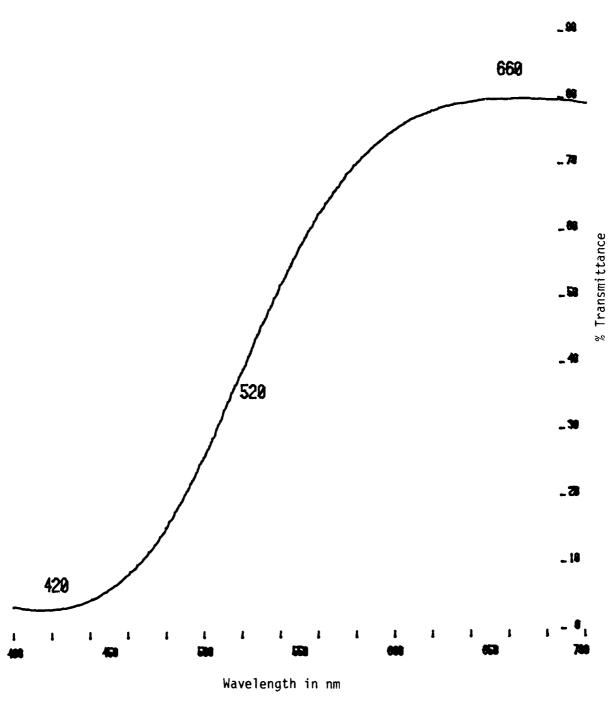


Figure 8. Transmittance of amber filter with Hunter D54.

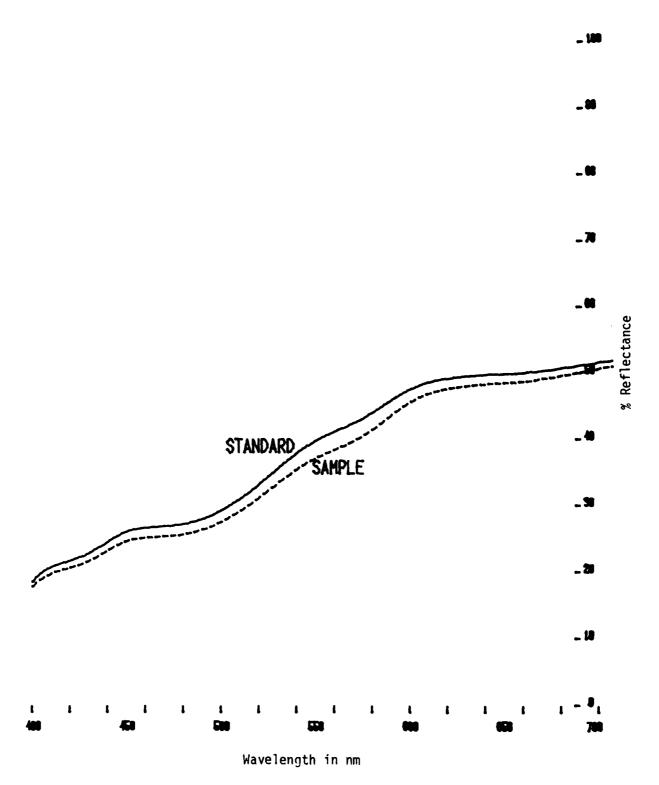


Figure 9. Reflectance curves of a pair of tan specimens with the Match-Scan.

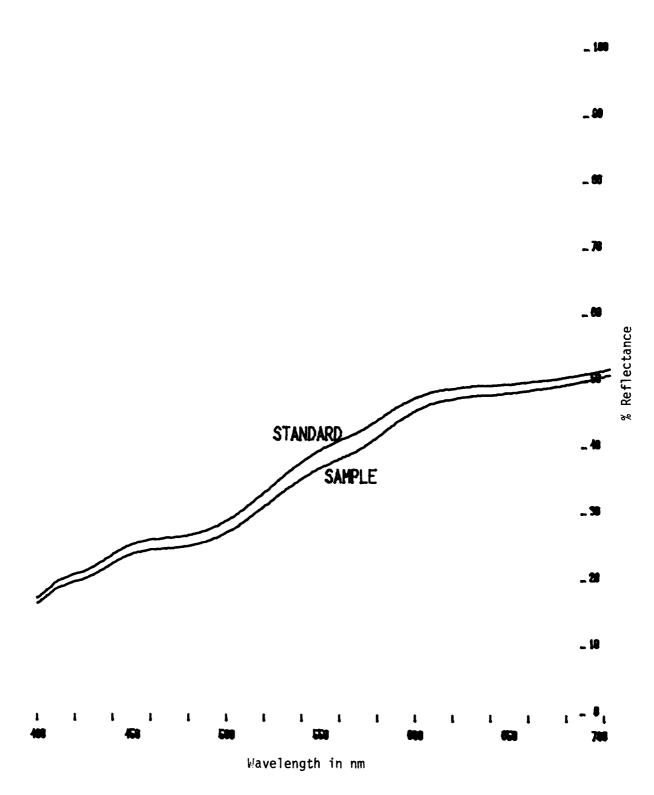


Figure 10. Reflectance curves of a pair of tan specimens with the Hunter D54.

.R QMSTAT DATE: 10/11/80

BEGIN WITH SAMPLE NO.?(2-5)

2

MEASURE: WHITE TILES INSERT SAMPLE THEN HIT RETURN

PAUSE --

W/L	FIRST	AVG OF 2	AVG OF 10	SIGMA
400	99.56	99.56	99,60	0.046
410	99.64	99.66	99.62	0.037
420	99.70	99.67	99.63	0.039
430	99.69	99.66	99.62	0.044
440	99.66	99.66	99.63	0.029
450	99.61	99.61	99.62	0.024
460	99.67	99.65	99.63	0.030
470	99.66	99.63	99.62	0.027
480	99.59	99.61	99.64	0.032
490	99.63	99.62	99.63	0.013
500	99.63	99.61	99.60	0.013
510	99.59	99.58	99.59	0.018
520	99.59	99.58	99.59	0.014
530	99.61	99.59	99.60	0.019
540	99.57	99.59	99.60	0.020
550	99.62	99.61	99.59	0.022
560	99.59	99.60	99.57	0.023
570	99.57	99.57	99.59	0.013
580	99.61	99.61	99.59	0.024
590	99.58	99.59	99.60	0.021
600	99.59	99.60	99.60	0.020
610	99.63	99.63	99.62	0.023
620	99.58	99.60	99.61	0.023
630	99.62	99.61	99.62	0.925
640	99.57	99.58	99.63	0.028
650	99.66	99.67	99.66	0.021
660	99.65	99.66	99.66	0.020
670	99.70	99.70	99.68	0.030
680	99.74	99.72	99.71	0.041
690	99.63	99.68	99.69	0.041
700	99.74	99.72	99.72	0.048
710	99.79	99.80	99.77	0.049
**		· · · - ·	• • • •	3.4.7

Figure 11. Statistical study for Match-Scan.

MEASURE:	AMBER FILTER	INSERT	SAMPLE	THEN	HIT	RETURN
PAUSE						

W/L	FIRST	AVG OF 2	AVG OF 10	SIGMA
400	3.99	3.98	3.98	0.009
410	3.53	3.54	3.53	0.007
420	3.52	3.53	3.52	0.007
430	3.94	3.94	3.95	0.005
440	4.88	4.88	4.88	0.005
450	6.44	6.44	6.44	0.006
460	8.73	8.74	8.74	0.005
470	11.84	11.85	11.86	0.007
480	15.92	15.91	15.90	0.009
490	21.01	21.01	21.01	0.008
500	26.81	26.81	26.81	0.010
510	32.80	32.81	32.82	0.010
520	39.17	39.18	39.20	0.012
530	45.61	45.63	45.62	0.011
540	51.84	51.83	51.82	0.007
550	57.48	57.49	57.51	0.013
560	62.54	62.53	62.55	0.014
570	66.88	66.86	66.84	0.022
580	70.43	70.43	70.43	0.015
590	73.27	73.27	73.28	0.024
600	75.52	75.51	75.49	0.017
610	77.14	77.13	77.11	0.019
620	78.28	78.27	78.28	0.015
630	79.06	79.07	79.08	0.027
640	79.65	79.63	79.59	0.017
650	79.84	79.84	79.85	0.016
660	79.94	79.96	79.97	0.016
670	79.94	79.95	79.93	0.025
680	79.69	79.71	79.73	0.029
690	79.50	79.47	79.47	0.034
700	79.11	79.08	79.07	0.031
710	78.49	78.53	78.54	0.028

Figure 11. Statistical study for Match-Scan (continued).

MEASURE: GRAY PORCELAIN INSERT SAMPLE THEN HIT RETURN
PAUSE --

W/L	FIRST	AVG OF 2	AVG OF 10	SIGMA
400	42.05	42.07	42.07	0.028
410	44.43	44.39	44.40	0.024
420	44.42	44.45	44.46	0.016
430	44.23	44.24	44.24	0.020
440	44.07	44.08	44.10	0.012
450	44.02	44.03	44.03	0.019
460	43.98	44.00	44.00	0.011
470	43.97	43.97	43.98	0.013
480	44.00	43.98	43.97	0.012
490	43.96	43.98	43.97	0.010
500	43.92	43.93	43.95	0.010
510	43.95	43.94	43.94	0.997
520	43.95	43.97	43.97	0.016
530	43.95	43.95	43.95	0.011
540	43.91	43.90	43.89	0.012
550	43.81	43.80	43.80	0.014
560	43.63	43.63	43.65	0.010
570	43.49	43.49	43.48	0.009
580	43.35	43.35	43.35	0.011
590	43.27	43.26	43.26	0.013
600	43.23	43.23	43.22	0.010
610	43.25	43.25	43.25	0.011
620	43.35	43.35	43.34	0.015
630	43.39	43.42	43.40	0.017
640	43.48	43.47	43.46	0.011
650	43.47	43.48	43.49	0.017
660	43.54	43.52	43.52	0.014
670	43.55	43.53	43.55	0.016
680	43.61	43.62	43.64	0.015
690	43.80	43.78	43.77	0.008
700	43.83	43.87	43.86	0.020
710	44.06	44.05	44.02	0.025

Figure 11. Statistical study for Match-Scan (continued).

MEASURE: STD TAN PLASTIC INSERT SAMPLE THEN HIT RETURN PAUSE ---

MEASURE: SPL TAN PLASTIC INSERT SAMPLE THEN HIT RETURN
PAUSE ---

STD	ONE	X= 0	.4249	Y= 0.	4023 Z	= 0.2	605
STD	AV2	X= 0	. 4249	Y= 0.	4023 Z	= 0.2	605
STD	AV10	x= 0	.4248	Y= 0.	4022 Z	= 0.2	605
are	SIG	X=0.0	00003	Y=0.0	0002 Z	=0.00	003
SPL	ONE	x= 0	. 4050	Y= 0.	3801 Z	= 0.2	459
SPL.	AV2	x= 0	4050	Y= 0.	3800 Z	= 0.2	459
SPL	AV10	X= 0	4048	Y= 0.	3799 Z	= 0.2	459
SPL	SIG	X=0.0	0010	Y=0.0	0010 Z	=0.00	007
STD	ONE	L*=	69.63	5 A*=	6.80	B*=	19.91
STD	AV2	L.*=	69.63	5 A*=	6.79	B*=	19.91
STD	AV10	L * =	69.63	S A*=	6.79	B*=	19.91
STD	SIG	L*=	0.002	*=	0.006	B*=	0.004
SPL	ONE	L*=	68.03	A*=	7.76	B*=	19.57
SPL	AV2	L*=	68.02	: A*=	7.76	B*=	19.57
SPL.	AV10	L*=	68.01	A*=	7.75	B*=	19.56
SFL	SIG	L*=	0.007	' A ≭ ≖	0.004	B*=	0.008
ONE DL	= 1.	61 DC	:= 0	.94 DI	E= 1	.86	
AV2 DL=	· 1.	61 DC	:= o	.95 D	E= 1	.87	
AV10 DL=	· 1.	62 DC	:= o	.94 DI	E= 1	.87	
SIG DL=	• 0.0	06 DC	= 0.	013 DE	E= 0.	014	

Figure 11. Statistical study for Match-Scan (continued).

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?$Q"STA1
 DATE: 10/14/80
  BEGIN WITH SAMPLE NO. 2(1-5)
```

- 1. ON HUNTER PRESS "TRANS", PUT WHITE TILE OVER PORT. BLOCK BEAM WITH BLACK CARDBOARD
- 2. PRESS "ZERO". REMOVE CARDBOARD
 3. PRESS "STDZ". AFTER "STANDARDIZED" PRINTS OUT ON HUNTER.
- 4. PRESS "ASCII"; THEN "2"
- 5. PRESS RETURN ON SPC-16 CONSOLE TAUSE

	• AMBER	FILTER	INSERT SAM	PLE.PRESS	READ ON	HUNTER, THEN	1 ONM
PAUSE							
N/L	FIRST	AVG OF 2	AVG OF 10	SIGMA			
400	3.99	3.97	3.96	0.019			
410	3.50	3.51	3.51	0.010			
420	3.50	3.50	3.50	0.005			
430	3.20	3,90	3.89 4.82	0.010			
440	4.82	4.82		0.004			
450	6.39	6.39	6.39	0.004			
460	8.57	8.57	8.57	0.005			
470 480	11.48	11.48 15.45	11.48 15.46	0.006 0.008		,	
490	20:46	20.46	20.45	0.010			
500	26.02	26.40	26.02	0.006			
510	32.18	32:16	32.16	0.005			
520	28,72	38.72	38.70	0,013			
530	45.02	45.02	45.03	0.013			
540	51.13	51.16	51.15	0.013			
550	56.92	56.92	56.90	0.014			•
530	61.95	61.96	61.95	0.014			
570	66.33	66.33	66.33	0.015			
580	70.14	70.14	70.12	0.015			
590	72.79	72.79	72.78	0.015			
600	75./20	75.20	75.19	0.015		•	
610	77,:19	77.19	77.19	0.014			
620	78.24	78.25	78.24	0.017			
630	79.00	79.01	78.99	0.029			
640 650	79.64 80.13	79.64 80.14	79.65 80.12	0.017 0.019			
630	50.15	80.16	80.12	0.016			
670	79.94	79.94	79.55	0.011			
680	79.96	79.96	79.97	0.014			
693	79.96	79.96	79.95	0.016			
700	79:52	79.52	79.50	0.019			
710	79.04	79.06	79.06	0.023			

Figure 12. Statistical study for Hunter D54.

W/L	FIRST	AVG OF 2	AVG OF 10	SIGMA
400	95.64	95.63	95:57	0.050
410	94.66	94.65	94.63	0.023
420	94.95	94.94	94.95	0.012
430	95.71	95.70	95.71	0.011
440	96.32	96.32	96.33	0.012
450	94.95	94.94	96.95	0.014
460	97.42	97.42	97.41	0.019
470	97.71	97.71	97.69	0.018
460	97.93	97.92	97.92	0.012
490	98.12	98.12	98.12	0.012
500	98.21	98.20	98.22	0.019
510	98:20	98.21	98.22	0.013
520	98.26	98.26	98.26	0.006 0.019
530	98:49	98.49	98.51	0.019
540	98.33	98.133	98.35	0.1020
550	98.35	98.35	98.36	0.010
540	98.26 98.34	98. ²⁴ 98. ³³	98.24	0.019
570 500			98.34	
580	93.27	98:26	98.27	0.011
520	98.45	98.45	98.46	0.013
600	98.16	98.14	98.14	0.014
610 620	98.14 98.08	98.14 98.06	98.15 98.06	0.019
630	93.16	98.14	98.14	0.016
640	98.18	98:17	98.18	0.009
650	98:15	98.14	98.17	0.018
660	98.09	98.08	98:10	0.015
670	98.19	98.19	98:20	0.011
680	97.97	97.97	97.97	0.007
690	98.21	98.21	98,20	0.007
700	98.11	98.10	98.10	0.014
710	97:94	97.94	97.98	0.028
			• •	

Figure 12. Statistical study for Hunter D54 (continued).

	GNAY P	ORCELAIN	INSERT SAMPI	LE,PRESS	READ	OH	HUNTER, THEN	1012
rauge ral	FIRST	AVG OF 2	AVG OF 10	STOKA				
400	39.25			SIGMA				
410	41.76	39.25 41.75	39.25	0.042				
420	42.20	42.19	41.77 42.21	0.019 0.018				
430	42.19	42.19	42.19	0.007				
440	42.31	42.31	42.32	0.007				
450	42.47	42.47	42.48	0.014				
460	42.70	42.70	42.72	0.013				
470	42.68	42,68	42.69	0.012				
480	42.76	42.76	42.76	0.005				
490	42.84	42.84	42.84	0.008			•	
500	42.87	42,86	42.85	0.011			•	
510	42.87	42.87	42.87	0.011				
520	43.01	43.01	43.01	0.008				
530	43.04	43.03	43.03	0.011				
540	42.92	42.92	42.93	0.017				
550 560	42.85 42.68	42.85	42.86	0.019				
		42.68	42.68	0.006				
570 580	42.42 42.28	42.42 42.28	42.43 42.29	0.014	•		•	
590	42.28	42.28	42.29	0.010				
600	42.14	42.14	42.14	0.006				
610	42.14	42.14	42.13	0.000				
620	42.10	42.10	42.11	o.oii				
630	42.25	42,25	42.26	0.013				
640	42.23	42.23	42.23	0.013				
6 50	42.33	42, 33	42.34	0.009				
660	42.39	42.39	42.40	0.011				
670	42.37	42.37	42.37	0.007				
080	42.53	42.53	42.55	0.009				
690 760	42.65	42.65	42.66	0.012				ı
700 710	42.80	42.80	42.79	0.010				
710	42.86	42.86	42.87	0.015				

Figure 12. Statistical study on Hunter D54 (continued).

MEASURE: SID TAN PLASTIC INSERT SAMPLE, PRESS READ ON HUNTER, THEN 10NM PAUSE

MUASURE: EDL CHE PLASTIC INSERT SANCLE, PRESS READ ON HUFTER, THEN TOP!! PAUSE

```
ONE X= 0.1127 Y= 0.2011 X= 0.2500
 Sill
       X72 Xc 0.4127 Y= 0.3911 Z= 0.2500
  57.7
       1710 X= 0.4127 Y= 0.3911 Z= 0.2500
 SID
       SIG Xm0.00003 Ym0.00002 Zm0.00000
 STO
 Sin
       0.99 \times 0.3927 \text{ Y= 0.3689 Z= 0.2358}
       AM2 - Km 0.3028 Ym 0.3690 Zm 0.2358
       AVIO X- 0.3900 Y= 0.3691 Z= 0.2358
 SPI.
 511
       SIG X:0,00000 Y=0,00008 Z=0,00005
 STO
       Office
            L*= 68.83 a*=
                             6.60 b*= 20.27
 5T7
       AV2 Lu= 63.83 am=
                             6.6! bt= 20,27
       AVIO Lx= 68.83 ax= 6.60 bx= 20.28
  STD
       GIG I. - 0.001 LA- 0.007 bt= 0.005
  STD
  SP".
       (119 Les 67.20 asm
                             7.54 b
                                       19.05
       1472 Lt - 67,20 eta
  S71.
                             7.54 b*=
                                       19.89
                                       19.90
  SP:
       AVIO Lan Ol. 21 name
                             7.54 bh=
 SP
       SIG 154 0,606 65+ 0.000 b*≈ 0.005
ONE DES
          1.13 77
                    Olab DE⇒
                                1.86
                                1.85
AV2 DL=
          1.60 NO - (.63 DE=
                               -1.85
AVIO DL
         1 62 PG 0 90 DE=
```

Figure 12. Statistical study of Hunter D54 (continued).

0.006 1.74 0.022 1.77 0.023

SIG DU STOP

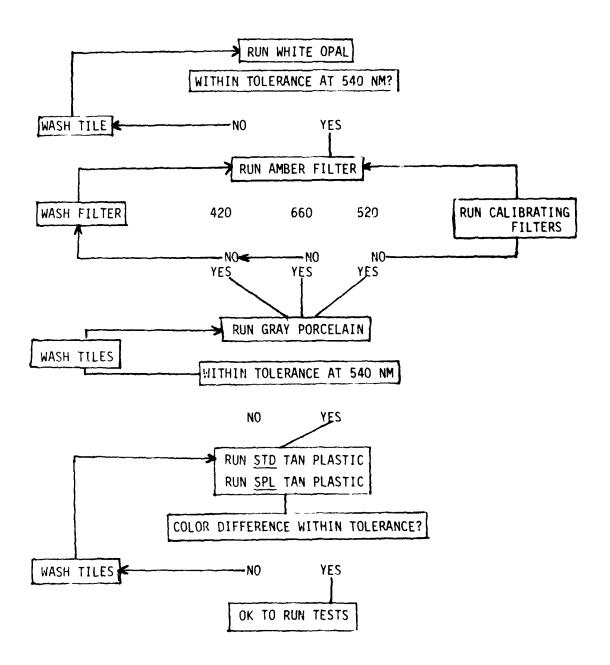


Figure 13. Schematic of standardization of Match-Scan.

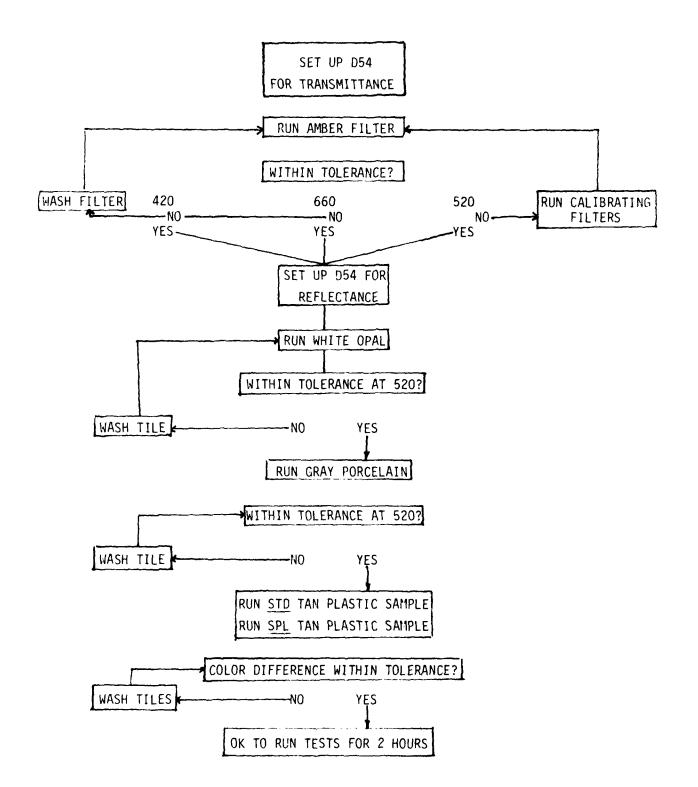


Figure 14. Schematic of standardization of Hunter D54.

DATE: 1/25/81

BEGIN WITH SAMPLE NO.?(1-5)

1

MEASURE: WHITE TILES INSERT SAMPLE THEN HIT RETURN AFTER PAUSE AT 540 NM UPPEV LIMIT 99.62 LOWER LIMIT 99.48 FAUSE --

W/L FIRST AVG OF 2 540 99.54 99.53

MEASURE: AMBER FILTER INSERT SAMPLE THEN HIT RETURN AFTER PAUSE AT 420 NM UPPER LIMIT 3.53 LOWER LIMIT 3.47 AT 520 NM UPPER LIMIT 39.27 LOWER LIMIT 38.93 AT 660 NM UPPER LIMIT 80.09 LOWER LIMIT 79.85 PAUSE ---

W/L.	FIRST	AVG OF 2
420	3.49	3.49
520	39.15	39.16
660	80.00	79.96

MEASURE: GRAY FORCELAIN INSERT SAMPLE THEN HIT RETURN AFTER PAUSE AT 540 NM UPPER LIMIT 44.00 LOWER LIMIT 43.80 PAUSE --

W/L FIRST AVG OF 2 540 43.92 43.94

MEASURE: STD TAN PLASTIC INSERT SAMPLE THEN HIT RETURN AFTER PAUSE COLOR DIFF. UPPER LIMIT 1.94 LOWER LIMIT 1.84
PAUSE ---

MEASURE: SPL TAN PLASTIC INSERT SAMPLE THEN HIT RETURN AFTER PAUSE PAUSE --

AVG OF 2 DL= 1.60 DC= 0.97 DE= 1.87 STOF --

Figure 15. Standardization test for Match-Scan, typical output from QMSTAN computer program.

```
?SOSTANH
  DATE: 1/27/84
DEGIT TITE SOUND MO.? (1-5)
  1. ON 054 PRESS "ASCII OUT", THEN "O", THEN "TRANS"
        PUT WHITE PORCELAIN OVER PORT.
  BLOCK BRAM WITH BLACK CARDBOARD
2. PRESS "ZERO". REMOVE CARDBOARD
  3. PPESS "STOZ". AFTER "STANDARDIZED" PRINTS OUT ON D54
4. PRESS "ASCII", THEN "2",
5. PRESS "RETURN" ON SPC+16 CONSOLE PRINTER
PAUSE
                                  INSERT SAMPLE IN D54;
  MEASURE: AMBER FILTER
    AFTER A PAUSE IS PRINTED, PRESS "READ" ON D54
    AFTER BELL RINGS, PRESS "TONY" AND "RETURN" AT SAME TIME
  AT 420 NU UPPER LIMIT 3.51 LOWER LIMIT 3.45
  AT 520 NY UPPER LIMIT 38.86 LOWER LIMIT 38.50
AT 660 NY UPPER LIMIT 80.32 LOWER LIMIT 80.08
 PAUSE
 PAUSE
?
            FIRST
                       AVG OF 2
  HIL
   420
              3.49
                           3.49
             33.76
                          38.74
   520
   660
             89.20
                          80.20
 *** RETOVE AMBER FILTER***
  1. OH 054, PRESS "ASCII", THEN "O", THEN "R-SIM"/
2. PRESS "ZERO". PUT WHITE PORCELAIM OVER PORT
                                                                   PUT ZEPO TRIB
  3. PHESS "STOZ". PUT GRAY PORCELAIN OVER PORT
  4. PRESS "STDZ". AFTER "STANDARDIZED" PRINTS OUT ON 054,
  5. PRESS "ASCII", THEN "2"
6. PRESS "RETURN" ON SPC-16 CONSOLE PRINTER
 PAUSE
  MEASURE: WHITE TILE
                                  INSERT SAMPLE IN D54;
     AFTER A PAUSE IS PRINTED, PRESS "READ" ON D54
    AFTER BELL RINGS, PRESS "10MM", AND "RETURN" AT SAME TIME
  AT 540 NM UPPER LIMIT 98.46 LOWER LIMIT 98.26
 PAUSE
?
 PAUSE
?
                       AVG OF 2
  WIL
            FIRST
   540
            98.40
                          98.40
```

Figure 16. Standardization test for Hunter D54, typical output from QSTANH computer program.

```
MEASURE: GRAY PORCELAIN : INSERT SAMPLE IN D54:
   AFTER A PAUSE IS PRINTED, PRESS "READ" ON D54
    AFTER BELL RINGS, PRESS "TONY" AND "RETURN" AT SAME TIME
 AT 540 NY UPPER LIMIT 43.06 LOWER LIMIT 42.86
PAUSE
?
PAUSE
         FIRST
                  AVG OF 2
 WIL
                    42.92
          42,92
 MEASURE: STO TAN PLASTIC INSERT SAMPLE IN D54:
   AFTER A PAUSE IS PRINTED, PRESS "READ" ON D54
   AFTER BELL RINGS, PRESS "TOHM" AND "RETURN" AT SAME TIME
 COLOR DIFFERENCE: UPPER LIMIT 1.93 LOWER LIMIT
PAUSE
?
PAUSE
 MEASURE: SPL TAN PLASTIC INSERT SAMPLE IN D54:
   AFTER A PAUSE IS PRINTED, PRESS "READ" ON D54
   AFTER BELL RINGS, PRESS "IONH" AND "RETURN" AT SAME TIME
PAUSE
PAUSE
           1.63 DC=
                      0.88 DE=
                                 1.85.
OHE THE
AVS DL=
           1.62 DC=
                      0.87 DE=
                                 1.84
***OK TO MAKE MEASUREMENTS***
STOP
```

Figure 16. Standardization test for Hunter D54 (continued).

```
?$OSTANH
  DATE# 1/27/81
  BEGIN WITH SAMPLE NO.? (1-5)
  1. OH D54 PRESS "ASCII OUT", THEN "O", THEN "TRANS"
       PUT WHITE PORCELAIN OVER PORT,
       BLOCK BEAM WITH BLACK CARDBOARD
  2. PRESS "ZERO". RETOVE CARDBOARD
  3. PRESS "STDZ". AFTER "STANDARDIZED" PRINTS OUT ON D54 4. PRESS "ASCII", THEN "2".
  5. PRESS "RETURN" ON SPC-16 CONSOLE PRINTER
 PAUSE
?
  MEASURE: AMBER FILTER INSERT SAMPLE IN D54:
AFTER A PAUSE IS PRINTED, PRESS "READ" ON D54
    AFTER BELL RINGS, PRESS "TONY" AND "RETURN" AT SAME TIME
  AT 420 RM UPPER LIMIT 3.51 LOWER LIMIT 3.45 AT 520 RM UPPER LIMIT 38.86 LOWER LIMIT 38.50
  AT 660 MM UPPER LIMIT 80.32 LOWER LIMIT 80.03
 PAUSE
 PAUSE
?
          FIRST
                    AVG OF 2
  W/L
                       3.77
   420
            3.76
 ***READING AT 420NY IS OUT OF SPECS FOR: AMBER FILTER
     WASH SAMPLE. THEN
  MEASURE: AMBER FILTER
                              INSERT SAMPLE IN D54:
    AFTER A PAUSE IS PRINTED, PRESS "READ" ON D54
    AFTER BELL RINGS, PRESS "1000" AND "RETURN" AT SAME TIME
  AT 420 NY UPPER LIMIT 3.51 LOWER LIMIT 3.45
  AT 520 NM UPPER LIMIT 38.86 LOWER LIMIT 38.50
  AT 660 NM UPPER LIMIT 80.32 LOWER LIMIT 80.08
PAUSE
PAUSE
                    AVG OF 2
  W/L
          FIRST
            3.48
                       3.48
   420
                      38.74
   520
            38.74
   660
           80.14
                      80.15
 *** RUTOVE APRICE FILTER***
  1. O. 054, PRESS "ASCHI", THEN "O", THEN "R-SIN"
                                                             PUT ZERO TRAP
  2. PRESS "ZERO". PUT SHITE PORCELAIN OVER PORT
  3. PRESS "STOZ". PUT GRAY PORCELAIN OVER PORT
  4. PRESS "STOK". AFTER "STAMBARDIZED" PRINTS OUT ON D54,
  5. Passs "Ascii", Than "2"
  6. PRESS "RETURN" ON SPC-16 CONSOLE PRINTER
 PAUSE
```

Figure 16. Standardization tests for Hunter D54 (continued).

APPENDICES

		P	ege?
Appendix	A.	Computer Program QMSTAT for Match-Scan Statistical Study.	41
Appendix	В.	Computer Program QMSTAT for Hunter D54 Statistical Study.	45
Appendix	C.	Computer Program QMSTAN for Standardization Program of Match-Scan.	49
Appendix	D.	Computer Program QSTANH for Standardization Program of Hunter D54.	53

Appendix A

Computer Program QMSTST for Match-Scan Statistical Study.

```
FRUGRAM UMSTAT
\boldsymbol{c}
        --- TO CALCULATE STATISTICAL DATA FOR A STANDARDIZATION
\mathbb{C}
        PROCEDURE APPLICABLE TO THE MATCH-SCAN
\mathbb{C}
C
        LINK INSTRUCTIONS:
C
        ASS DX1 DK
\epsilon
        R LINK
\mathbf{C}
        *QMSTAT=QMSTAT,DXO:MSLIB,FISNOV.NEW
\mathbb{C}
C
        DIMENSION AVGNO(4), CMF(3,32), D65(32), FAC(32,3), FACT(32), FLAS(
        DIMENSION R(32,10),RC(32,13,2),RG(32),STAR(3,13,2),SPL(4,5)
        DIMENSION TRI(3,13,2), TRIO(3), VAL(3), DSQ(3), AVG(3), CD(3,13)
      DATA CMF/0.0191,0.0020,0.0860
         0.0847,0.0088,0.3894
     Хy
     Хv
         0.2045,0.0214,0.9725
         0.3147,0.0387,1.5535
     Χv
         0.3837,0.0621,1.9673
     χ,
         0.3707,0.0895,1.9948
     Χ,
     Χ,
         0.3023,0.1282,1.7454
     Хy
         0.1956,0.1852,1.3176
     Хy
         0.0805,0.2536,0.7721
         0.0162,0.3391,0.4153
     Хy
         0.0038,0.4608,0.2185
     Χ,
         0.0375,0.6067,0.1120
     Хy
     Χy
         0.1177,0.7618,0.0607
     Хy
         0.2365,0.8752,0.0305
     Хy
         0.3768,0.9620,0.0137
     Χy
         0.5298,0.9918,0.0040
         0.7052,0.9973,0.0000
     Хy
         0.8787,0.9556,0.0000
     Хy
     Χ,
         1.0142,0.8689,0.0000
     Хy
         1.1185,0.7774,0.0000
         1.1240,0.6583,0.0000
     Хy
         1.0305,0.5280,0.0000
     Χ,
         0.8563,0.3981,0.0000
     Χø
         0.6475,0.2835,0.0000
     Χ,
     Χy
         0.4316,0.1798,0.0000
         0.2683,0.1076,0.0000
     Χ'n
         0.1526,0.0603,0.0000
     Χy
         0.0813,0.0318,0.0000
     Χ,
         0.0409,0.0159,0.0000
     Χv
     Χy
         0.0199,0.0077,0.0000
     Χ.
         0.0096,0.0037,0.0000
     Χ.
         0.0046,0.0018,0.0000/
        DATA D65/828.,916.,935.,868.,1049.,1171.,1178.,1149.,1159.,1080
         1094.,1078.,1049.,1077.,1044.,1040.,1000., $\\\4.,957.,886.
     χ,
         900.,896.,876.,833.,837.,800.,802.,822.,783.,697.,716.,743./
     χ,
        DATA SPL//WHIT/, 'E TI/, 'LES ', '
                                              /,/AMBE/,/R FI/,/LTER/,/
        'GRAY',' POR','CELA','IN ','STD ','TAN ','FLAS','TIC ','SPL ',
        'TAN ','PLAS','TIC '/
        DATA AVGNO,PLAST/10NE 1,1AV2 1,1AV101,1SIG1,1STD 1, 3PL 1/
        FORMAT(' DATE: '12,2('/',12))
100
```

FORMAT('\$ BEGIN WITH SAMPLE NO.?(2-5)',6E)

150

Appendix A (continued)

```
200
         FORMAT('OMEASURE: '4A4,' INSERT SAMPLE THEN HIT RETURN'/)
         FORMAT(I5,3F10.2,F10.3)
300
         FORMAT(1H0,2(2X,A4), / X=',F7.4, / Y=',F7.4, / Z=',F7.4)
400
         FORMAT(1H0,2(2X,A4), / X=/,F7.5, / Y=/,F7.5, / Z=/,F7.5)
450
         FORMAT( / W/L/,5X, /FIRST/,4X, /AVG OF 2/,2X, /AVG OF 10/,4X, /SIGMG/ -
500
         FORMAT(1H0,2(2X,A4), L*=',F7,2,' A*=',F7,2,' B*=',F7,2)
600
         FORMAT(1H0,2(2X,A4), / L*=/,F7.3, / A*=/,F7.3: / B*=/,F7.3)
650
         FORMAT(1H0,A4, DL=(,F7.2, DC=(,F7.2, DE=(,F7.2)
200
250
         FORMAT(1H0,A4, DL=',F7.3, DC=',F7.3, DE=',F7.3)
         CALL IDATE(IM, ID, IY)
         WRITE(5,100) IM, ID, IY
         WRITE(5,150)
        READ(5,300) NSAM
         DO 2000 II=1,5
         IF(II.EQ.1) GOTO 960
         IF(II.LT.NSAM) GOTO 2000
960
         I = II
         WRITE(5,200) (SPL(M,I),M=1,4)
         PAUSE
         DO 1000 N=1,10
         DO 980 L=1.32
980
         FACT(L)=1.
         CALL GMSR(4000,7100,100,1,0,5,0,1,FACT,RG,(ER)
         DO 990 L=1,32
         R(L,N)=RG(L)
990
         CALL IDLE(1000)
1000
         CONTINUE
         IF(I.LT.4) WRITE(5,500)
         IF(I.GT.1) GOTO 1100
         DO 1040 L=1,32
         FAC(L,2)=0.
        FAC(L,3)=0.
         DELSQ=0.
         DO 1020 N=1+10
         IF(N.EQ.1) FAC(L,1)=R(L,N)
         IF(N.LE.2) FAC(L.2)=R(L.N)*0.5 + FAC(L.2)
        FAC(L_13)=R(L_1N)*0.1 + FAC(L_13)
1020
        CONTINUE
         100 1030 N=1,10
1030
         DELSQ=(R(L_1N)-FAC(L_13))*(R(L_1N)-FAC(L_13)) - DELSQ
         SIGMA=SQRT(DELSQ*0.1111)
        WRITE(5,300) 390+L*10,(FAC(L,M),M=1,3),SIGMA
        DO 1035 M=1.3
1035
        FAC(L,M)=FAC(L,M)*0.01
1040
        CONTINUE
        GOTO 2000
1100
        DO 1140 L=1,32
        VAL(2)=0.
        VAL(3)=0.
        DELSQ=0.
        DO 1120 N=1,10
         IF(N.EQ.1) VAL(1)=R(L,N)/FAC(L,1)
         IF(N.EQ.1.AND.I.GE.4)RC(L.1.I-3)=VAL(1)
         IF(N.LE.2) VAL(2)=R(L,N)*0.5/FAC(L,2)+VAL(2)
```

Appendix A (continued)

```
IF(N.EQ.2.AND.1.GE.4) RC(L,2,1-3)=VAL(2)
        R(L_1N) = R(L_1N) / FAC(L_13)
        VAL(3)=R(L_1N)*0.1 + VAL(3)
        IF(I.GE.4) RC(L.3.I-3)=VAL(3)
         IF(I,GE,4) RC(L,3+N,I-3)=R(L,N)
1120
        CONTINUE
         IF(I.GE.4) GOTO 1140
        DO 1130 N=1,10
        DELSQ=(R(L,N)-VAL(3))*(R(L,N)-VAL(3)) + DELSQ
1130
        SIGMA=SQRT(DELSQ*0.1111)
        WRITE(5,300) 390+L*10,(VAL(M),M=1,3),SIGMA
1140
        CONTINUE
2000
        CONTINUE
C
        I IS THE TRISTIMULUS COUNTER
C.
        J IS THE AVERAGES COUNTER
\mathbf{c}
        K IS THE SAMPLE NUMBER OF THE PLASTIC CHIPS COUNTER
\mathbf{C}
        L IS THE WAVELENGTH COUNTER
        DO 2900 I=1,3
        TRIO(I)=0.
        DO 2900 L=1,32
2900
        TRIO(I)=TRIO(I)+100.*CMF(I,L)*D65(L)
        TH=1./3.
        DO 3070 K=1,2
        J1 = 1
        J3=3
        DO 2970 I=1,3
2970
        AVG(1)=0.
2980
        DO 3050 J≈J1,J3
        DO 3020 I=1,3
        TRI(I,J,K)=0.
        DO 3000 L=1,32
        TRI(I,J,K)=TRI(I,J,K) + RD(L,J,K)*CMF(I,L)*DASA(L)
3000
        CONTINUE
3020
        TRI(I,J,K)=TRI(I,J,K)/TRIQ(I)
        IF(J1.6T.3) GOTO 3030
        WRITE(5,400) PLAST(K),AUGND(J),(TRI(M,J,K),M=1,3)
        GOTO 3050
3030
        DO 3040 I=1,3
        AVG(I) = AVG(I) + TRI(I + J + K) * O + 1
3040
        CONTINUE
3050
        CONTINUE
        IF(J1.EQ.4) GOTO 3060
        11=4
        J3=13
        GOTO 2980
3060
        DO 3068 I=1,3
        DSQ(I)=0.
        DO 3065 J=4+13
3065
        DSQ(I) = (TRI(I + J + K) - AVG(I)) * (TRI(I + J + K) - AVG(I)) + DSQ(I)
        DSQ(I)=SQRT(DSQ(I)*0.1111)
3068
        CONTINUE
        WRITE(5,450) PLAST(K), AVGND(4), (DSQ(I), I=1,3)
3070
        CONTINUE
        DO 3080 I=1.3
        DO 3080 J=1,13
        DO 3080 K=1+2
```

Appendix A (continued)

```
3080
        TRI(I,J,K)=TRI(I,J,K)**TH
        DO 3170 K=1,2
        J1 == 1
        J3#3
        DO 3100 I=1,3
3100
        AVG(I)=0.
3110
        DO 3150 J=J1,J3
        STAR(1,J,K)=116.0*TRI(2,J,K)-16.0
        STAR(2,J,K)=500.*(TRI(1,J,K)-TRI(2,J,K))
        STAR(3,J,K)=200.*(TRI(2,J,K)-TRI(3,J,K))
        IF(J1.GT.3) GOTO 3130
        WRITE(5,600) PLAST(K),AVGNO(J),(STAR(M,J,K),H=1,3)
        GOTO 3150
3130
        DO 3140 I=1,3
3140
        AVG(I)=AVG(I)+STAR(I,J,K)*0.1
3150
        CONTINUE
        IF(J1.EQ.4) GOTO 3160
        J1.≕4
        J3 = 13
        GOTO 3110
3160
        DO 3168 I=1,3
        DSQ(I)=0.
        DO 3165 J=4,13
        DSQ(I)=(STAR(1,J,K)-AVG(I))*(STAR(1,J,K)-AVG( )) +DSQ(I)
3165
        DSQ(I) = SQRT(DSQ(I) * 0.1111)
3168
        CONTINUE
        WRITE(5,650) PLAST(K), AVGNO(4), (DSQ(I), I=1,3)
3170
        CONTINUE
        J1=1
        J3:::3
        DO 3175 I=1,3
3175
        AVG(I)=Q.
3180
        DO 3250 J=J1,J3
        DO 3200 I=1,3
        STAR(I,J,1)=(STAR(I,J,2)-STAR(I,J,1))*(STAR(I,J,2)-STAR(I,J,1))
3200
        CII(1+J) = SQRT(STAR(1+J+1))
        CD(2,J) = SQRT(STAR(2,J,1) * STAR(2,J,1) + STAR(3,J,1) * STAR(3,J,1)
        CD(3,J)=SQRT(CD(1,J)*CD(1,J) + CD(2,J)*CD(2,J))
        IF(J1.GT.3) GOTO 3230
        WRITE(5,700) AVGNO(J),(CD(M,J),M=1,3)
        GOTO 3250
        DO 3240 I=1,3
3230
        AVG(I) = AVG(I) + CI(I,J) * 0.1
3240
3250
        CONTINUE
        TF(J1.NE.1) GOTO 3260
        J1 = 4
        J3=13
        GOTO 3180
        DO 3268 I=1,3
3260
        DSQ(I)=0.
        DO 3265 J=4,13
        DSQ(I) = (CD(I,J) - AVG(I)) * (CD(I,J) - AVG(I)) + DSQ(I)
3265
        DSQ(I)=SQRT(DSQ(I)*0.1111)
3268
        CONTINUE
        WRITE(5,750) AUGNO(4),(DSQ(M),M=1,3)
        STOP
4000
        END
                                     44
```

Appendix B.

Computer program QMSTAT for Hunter D54 statistical study.

```
?$COPY.DS(GMSTAT).TY
         PROGRAM QMSTAT
CC
            -10 CALCULATE STATISTICAL DATA FOR A STANDARDIZED PROCEDURE
C
         APPLICABLE TO THE HUNTER D54P SPECTROPHOTOMETER
         DIMENSION AVGNO(4), CMF (3,32), D65(32), FAC(32,3), PLAST(2)
         DIMENSION R(32,10), RC(32,13,2), RG(32), STAR(3,13,2), SPL(4,5)
         DIMENSION TRI(3,13,2),TRIO(3),VAL(3),DSQ(3),AVG(3),CD(3,13)
         DIMENSION NUL(32)
         DATA CMF/0.0191,0.0020,0.0860,0.0847,0.0088,0.3894
       -,0.2045,0.0214,0.9725,0.3147,0.0387,1.5535
       -.0.3837,0.0621,1.9673,0.3707,0.0895,1.9948
       -,0.3023,0.1232,1.7454,0.1956,0.1852,1.3176
       -.0.0305,0.2530,0.7721,0.0162,0.3391,0.4153
       -,0.0038,0.4608,0.2185,0.0375,0.6067,0.1120
       -,0.1177,0.7618,0.0607,0.2365,0.8752,0.0305
       -,0.3768,0.9620,0.0137,0.5298,0.9918,0.0040
       -,0.7052,0.9973,0.0000,0.8787,0.9556,0.0000
       -,1.0142,0.8689,0.0000,1.1185,0.7774,0.0000
      -,1.1240,0.6583,0.0000,1.0305.0.5280,0.0000
-,0.8563,0.3981,0.0000,0.6475,0.2835,0.0000
       -,0.4316,0.1798,0.0000,0.2683,0.1076,0.0000
       -,0.1526,0.0603,0.0000,0.0813,0.0318,0.0000
       -,0.0409,0.0159,0.0000,0.0199,0.0077,0.0000
       -,0.0096,0.0037,0.0000,0.0046,0.0018,0.0000/
      DATA D65/823.,916.,935.,868.,1049.,1171.,1178.,1149.,1159.,1088.,-1094.,1078.,1049.,1077.,1044.,1040.,1000.,964.,957.,886.,
      -900.,896.,876.,833.,837.,800.,802.,822.,783.,697.,716.,743./
DATA SPL/WHIT', E TI', LES ', 'AMBE', R FI', LTER',
       -'GRAY', POR', CELA', 'IN ', STD ', TAN ', PLAS', TIC', SPL ',
       -TAN / PLAS/ TIC //
         DATA AVGNO.PLAST/'ONE ','AV2 ','AV10','SIG','STD ','SPL '/
FORMAT(' DATE: ',12,2('/',12))
 100
         FORMAT( BEGIN WITH SAMPLE NO.?(1-5) .. 6X)
 150
         FORMAT(// MEASURE: '4A4.' INSERT SAMPLE, PRESS READ ON HUNTER, THEM
 200
        300
         FORMAT(15.3F10.2,F10.3)
         FORMAT(/2(2XA4), / X=/,F7.4, / Y=/,F7.4, / Z=/,F7.4)
 350
 400
         FORMAT(/2(2XA4), / X=/,F7.5, / Y=/,F7.5, / Z=/,F7.5)
FORMAT(/ W/L/,5X,/FIRST/,4X,/AVG OF 2/,2X,/AVG OF 10/,4X,/SIGMA/)
 450
 500
         FORMAT(/2(2XA4), L*=',F7.2, a*=',F7.2, b*=',F7.2)
FORMAT(/2(2XA4), L*=',F7.3, a*-',F7.3, b*=',F7.3)
 600
 650
         FORMAT(/A4. DL=',F7.2. DC=',F7.2. DE=',F7.2)
FORMAT(/A4. DL=',F7.3. DC=',F7.3. DE=',F7.3)
 700
 750
         CALL DATESB(IY.IM.ID)
         WRITE(5,100) IN.ID.IY
         WRITE(5,150)
         READ(5,350) HSAH
             GAM.GT.I) GOTO 950
         WRITE(5,150)
 950
         DO 2000 II=1.5
```

Appendix B (continued)

```
IF(II.LT.NSA'D GOTO 2000
900
         maiTe(5,200) (SPL(M,1),M=1,4)
         DO 1000 H=1.10
         PAUSE
         DO 980 L=1,32
READ(14,350) NWL(L),RG(L)
980
         CONTINUE
         DO 935 L=1,32
         \mathbb{E}(\mathbb{L}_{+}\mathbb{H}) = \mathbb{E}G(\mathbb{L})
935
         CONTINUE
1000
         IF (I.LT.4) WRITE(5,500)
         IF(I.Gr.1) GOTO 1100
         DO 1040 L=1,32
        FAC(L,2)=0
        FAC(L,3)=0
         DELSO=O.
         D0 1020 d=1,10
         IF(N.EQ.1) FAC(L.1)=R(L.N)
         IF(N.LE.2) FAC(L,2)=R(L,N)*0.5+ FAC(L,2)
        FNC(L,3)=B(L,N)*0.1 + FAC(L,3)
COUTINUE
1020
         D) 1030 H=1,10
         DELSO = (R(L, H) - FAC(L, 3)) * (R(L, N) - FAC(L, 3)) + DELSO
1030
         SIGMA=SORT(DELSQ*0.1111)
        NY=390+L+10
        MRITE(5,300) NM, (FAC(L,M), M=1,3), SIGMA D0 1035 M=1,3
1035
        FAC(L, H) = FAC(L, H) *0.01
1040
        CONTINUE
        GUTO 2000
1100
         D) 1140 L=1.32
        VLL(2)=0.
        VL(3)=0.
        DELSO=0.
        DO 1120 N=1.10
        IF(N.EO.1) VAL(1)=R(L,N)/FAC(L,1)
        IF(V.EQ.1.AND.I.GE.4) RC(L,1,I-3) = VAL(1)
        IE(V.LE.2) VAL(2)=R(L.N)*0.5/FAC(L.2)*VAL(2)
IE(V.E).2.AND.I.GE.4) RC(L,2,I-3)=VAL(2)
        R(L,H) = R(L,H) / FAC(L,3)
        VAL(3) = R(L, H) \times 0.1 + VAL(3)
        I^{\circ}(I_{\bullet}G_{\bullet}^{\circ},4) : \exists C(L_{\bullet}3,I_{\bullet}3)=VAL(3)
        IF(I.OE.4) RC(L,3+N,I-3)=R(L,N)
        CONTINUE
IF(I.CZ.4) GOTO 1140
1120
        a: 1130 H=1,10
1130
        DILION-(R(L,N)-VAL(3))*(R(L,N)-VAL(3))+DELSO
        SIGMA=SORT(DELSORO.1111)
        R (=370+L%10
```

Appendix B (continued)

```
TRITE(5,300) PM, (VAL CM), M=1,3), SIGMA COURTINUE
1140
2000
         Colon Line
         I IS THE TRISTIMULUS COUNTER
C
         J IS THE AVERAGES COUNTER K IS THE SAMPLE NUMBER OF THE PLASTIC CHIPS COUNTER
C
C
C
         L IS THE MAYELENGTH COUNTER SO 2900 I=1.3
        TRIO(I)=0.
DD 2200 L=1,32
TRIO(I)=TRIO(I)+100.*CMF(I,L)*D65(L)
THE1./3.
2900
         DD 3070 K=1.2
         JI=1
         J3≈3
D0 2070 I≈1,3
        AV3(I)=0.
D0 3050 J=J1,J3
2970
2980
        DJ 3020 I=1.3
TAI(!,J,K)=0.
        3000
3020
         IF(J1.0T.0) GOTO 3030
        UNITE(5,400) PLAST(K), AVGNO(J), (TRI(M, J, K), M=1,3)
GUTO 3000
3030
         DJ 3040 I=1,3
         AVG(I)=AVG(I)+TRI(I,J,K)+O.1
         CHITHUE
3040
3050
         ĬĒ(JI.ĒÖ.4) GOTO 3060
         J1:=4
         J3:=13
        GUTO 2930
3060
         .)) 3963 I≃1.3
         DBA(I)=0.
        00 3065 J=4,13
        \texttt{PPR}(I) = (\texttt{TRI}(I,J,K) - \texttt{AVG}(I)) * (\texttt{TRI}(I,J,K) - \texttt{AVG}(I)) + \texttt{DSQ}(I)
3065
        DUD(I)=SQRT(DSQ(I)*0.1111)
        C NOTIFIED (5,450) PLAST(K), AVGNO(4), (DSO(1), I=1,3) C NOTIFIED (5,250) I=1,3
3068
3070
         33 3000 J#1,13
            ાં છે છે K=1,2
3030
         TNI([,J,K)=<u>ŤŖI(I,J,K)**TH</u>
         170 %=1,2
        11:1
        J2::3
        JJ 3100 I≈1.3
```

Appendix B (continued)

```
ANGOIDEO.
3100
                                         00 0150 J=J1,J3

07.11(1,J,K)=116.0*TRI(2,J,K)=16.0

07.11(2,J,K)=800.*(TRI(2,J,K)=TRI(2,J,K))

07.11(3,J,K)=200.*(TRI(2,J,K)=TRI(3,J,K))
3110
                                         0070-0150
                                         Dr 3140 I=1.3
3130
                                         A ANGID = ANG(I) + STAR(I, J, K) *0.1
3140
3150
                                           IF(J(.E0.4) GOTO 3160
                                          J1 =4
                                          J0=13
0.770 3110
                                         1 3160 I=1.3
NCC(I)=0.
3160
                                         Ind 3165 J=4.13
DID((I)=(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*DSQ(I)
DID((I)=(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I,J,K)-AVG(I))*(STAR(I
3165
                                                 3%(I)=50MT(DSQ(İ)+0.1111)
WIINUH
3168
                                           ULITY (5, 450) PLAST(K), AVGNO(4), (DSQ(I), I=1,3)
3170
                                         J1=1
J2=3
                                            DA 3175 I=1.3
3175
                                                          3250 J=J1.J3
3200 I=1.3
3180
                                          STAB(I,J,1)=(STAR(I,J,2)-STAR(I,J,1))*(STAR(I,J,2)-STAR(I,J,1))
3200
                                         CD(),J)=SCRT(STAR(1,J,1))
                                             C1(2,J)=S1T(STAR(2,J,1)*STAR(2,J,1)+STAR(3,J,1)*STAR(3,J,1))
                                         C^{-}(3,J)=(C^{-}(1,J)*C^{-}(1,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,J)*C^{-}(2,
                                         IT(JE.GT.C) GOTO 3230
UNITE(5,700)AVGHO(J),(CD(M,J),M=1,3)
                                          0070 3250
                                         Un 0240 J=1.3
AVO(I)=AVO(I)+CD(I,J)*0.1
CAUTINUE
IF(U1.UE.1) GOTO 3260
 3230
 3240
 3250
                                           31::4
                                            J3#13
                                          GUTO 3180
                                                  ે 3000 J#1,3
3260
                                             :(<u>[</u>])=0.
                                           1.1 0265 J≈4,13
                                                 CD(I) = (CD(I,J) - AVG(I)) * (CD(I,J) - AVG(I)) + DSQ(I)
 3.205
                                        ANGLISSOUT(DSQ(I)*0.1111)
C NTIMUE
NTIMUE (5,750) AVGHO(4), (DSQ(M),M≈1,3)
 3208
4000
                                           ...)
```

Appendix C

Computer Program QMSTAN for Standardization Program of Match-Scan.

```
PROGRAM QMSTAN
        ---TO PROVIDE A STANDARDIZATION
        PROCEDURE APPLICABLE TO THE MATCH-SCAN
0
        LINK INSTRUCTIONS:
1
        ASS DX1 DK
        R LINK
        *@MSTAN=@MSTAN,DXO:MSLIB,FISNOV.NEW
C
C
\mathbf{C}
        DIMENSION CMF(3,32),D65(32),FAC(32,3),FACT(32)
        DIMENSION R(32,10), RC(32,2,2), RG(32), STAR(3,2,2), SPL(4,5)
        DIMENSION UL(6), OW(6), NM(5), AC(6)
        DIMENSION TRI(3,2,2), TRIO(3), VAL(3), CD(3,2)
      DATA CMF/0.0191,0.0020,0.0860
         0.0847,0.0088,0.3894
     Хy
         0.2045,0.0214,0.9725
     Χ,
     Χy
         0.3147,0.0387,1.5535
     Χy
         0.3837,0.0621,1.9673
     Χy
         0.3707,0.0895,1.2948
         0.3023,0.1282,1.7454
     Χ»
         0.1956,0.1852,1.3176
     Χv
     X
         0.0805,0.2536,0.2721
     Χy
         0.0162,0.3391,0.4153
     Χ.
         0.0038,0.4608,0.2185
     Χ,
         0.0375,0.6067,0.1120
     Χ'n
         0.1177,0.7618,0.0607
     Χ,
         0.2365,0.8752,0.0305
     Χy
         0.3768,0.9620,0.0137
     Χ×
         0.5298,0.9918,0.0040
     Χ,
         0.7052,0.9973,0.0000
     X,
         0.9787,0.9556,0.0000
     χ,
         1.0142,0.8689,0.0000
         1.1185,0.7774,0.0000
     Χ,
     Χ,
         1.1240,0.6583,0.0000
     Χy
         1.0305,0.5280,0.0000
     х,
         0.8563,0.3981,0.0000
     χ,
         0.6475.0.2835.0.0000
     χ,
         0,4316,0,1798,0,0000
     Χ×
         0.2683,0.1076,0.0000
     Χ,
         0.1526.0.0603.0.0000
     Χ,
         0.0813,0.0318,0.0000
     Х,
         0.0409,0.0159,0.0000
     Χ,
         0.0199,0.0077,0.0000
     Х•
         0.0096,0.0037,0.0000
         0.0046,0.0018,0.0000/
     Χ·
        DATA D65/828.,916.,935.,868.,1049.,1171.,1178.,1149.,1159.,1088.
     χ,
         1094.,1078.,1049.,1077.,1044.,1040.,1000.,964.,957.,886.
```

DATA SPL//WHIT/ , 'E TI', 'LES ', '

'GRAY',' POR','CELA','IN 'TAN ','PLAS','TIC '/

900,,896,,876,,833,,837,,800,,802,,822,,783,,697,,716,,743,/

// AMBE() 'R FI() 'LTER() (

','STD ','TAN ','PLAS','TIC ','SPL ',

Appendix C (continued)

```
\mathbb{C}
        1=0PAL@540;2=AMBER@420;3=AMBER@520;4=AMBER@440;5=GRAY@540;6=COL_DIF
        DATA NM/540,420,520,330,540/
        DATA UL/99.62.3.53.39.27.80.09.44.00.1.94/
        DATA OW/99,49,3,47,38,93,79,85,43,80,1,84/
                 ACZYUPPE', 'R LI', 'MIT ', 'LOWE', 'R LI', 'MIT '/
        DATA
        FORMAT(' DATE: '12,2('/',12))
100
        FORMAT('$ BEGIN WITH SAMPLE NO.?(1-5)',6X)
150
160
        FORMAT( AT (+14+ NM (+2(1X3A4+F6.2))
170
        FORMAT(/ COLOR DIFF,/,2(1X3A4,F6.2))
0175
                     CHANGE LIMITS? O=NO; 1=YES',4X}
        FORMAT('$
        FORMAT(2X3A4,/?/)
180
190
        FORMAT(F7.2)
        FORMAT( 'OMEASURE: '464,
200
        INSERT SAMPLE THEN HIT RETURN AFTER PAUSE()
        FORMAT('0***READING AT', 15, ' NM IS OUT OF SPECS FOR: ',4A4,/
510
     Χ′
            WASH SAMPLE, THEN/)
        FORMAT('*** COLOR DIFFERENCE IS OUT OF SPECS'/
220
     X'
               WASH PLASTIC TILES, THEN')
        FORMAT(I5,3F10,2,F10,3)
300
        FORMAT( / W/L/,5X, /FIRST/,4X, /AVG OF 2/)
500
        FORMAT(1HO, 'AVG OF 2 DL=',F7.2,' DC=',F7.2,' DE=',F7.2)
200
        CALL IDATE(IM, ID, IY)
        WRITE(5,100) IM, ID, IY
        切磨ますだ(ちょまちの)
        READ(5,300) NSAM
250
        DO 2000 I=1.5
        IF (I.NE.1.AND.I.LT.NSAM) GOTO 2000
260
        WRITE(5,200) (SPL(M,I),M=1,4)
        IF(I.EQ.5) GOTO 975
        TE(I.LE.2) K=0
        IF(I,GE.3) K=2
        IF(I.EQ.4) GOTO 970
        WRITE(5,160) NM(I+K), (AC(M), M=1,3), UL(I+K), (AC(M), M=4,6), OW(I+K)
97.5
        IF(I.EQ.4) WRITE(5,170) (AC(M),M=1,3),UL(6),(AC(M),M=4,6),OW(6)
970
Û
        WRITE(5,175)
Υī
        READ(5,300) ICH
        IF(TCH.EQ.O) GOTO 972
Ü
        WRITE(5,180) (AC(M),M=1,3)
Ð
\mathbf{D}
        READ(5,190) UL(I+K)
Ð.
        URITE(5,180) (AC(M),M=4,6)
        READ(5,190) OW(I+K)
Ţ1
072
        IF(I.NE.2) GOTO 975
        IF(K.LT.3) Kek+1
        IF(K.LT.3)GOTO 965
975
        CONTINUE
        PAUSE
        DO 1000 N=1,2
        DO 980 L=1,32
980
        FACT(L)=1.
        CALL GMSR(4000,7100,100,1,0,5,0,1,FACT,RG,IER)
        TO 990 L=1,32
990
        R(LyN)#RG(L)
        CALL TRLE(1000)
        CONTINUE
1000
```

Appendix C (continued)

```
1F(1.L1.4) WRITE(5,500)
        TF (I.GT.1) GOTO 1100
        ## 1040 L=1,32
        FAC(Ly2) #0;
        DO 1020 N=1,2
        IF(N.EQ.1) FAC(L.1)=R(L.N)
        IF(N.LE.2) FAC(L.2)≈R(L.N)*0.5 4 FAC(L.2)
1020
        CONTINUE
        IF(L.NE.15) GOTO 1030
                WRITE(5,300) 390+L*10,(FAC(L,M),M=1,2)
        IF(FAC(15,2).LT.UL(1).AND.FAC(15,2).GT.OW(1)) GOTO 1030
        WRITE(5,210) 540, (SPL(M,1), M=1,4)
        GOTO 960
1030
        DO 1035 M=1,2
1035
        FAC(L,M)=FAC(L,M)*0.01
1040
        CONTINUE
        GOTO 2000
1100
        DO 1500 L=1,32
        VAL(2)=0.
        DO 1120 N=1,2
        TF(N,EQ.1) VAL(1)=R(L,N)/FAC(L,1)
        IF(N.EQ.1.AND.I.GE.4)RO(L.1.I-3)=VAL(1)
        IF(N.LE.2) VAL(2)=R(L.N)*0.57FAC(L.2)+VAL(2)
        IF(N.EQ.2.AND.1.GE.4) RC(L.2.1-3)=VAL(2)
1120
        CONTINUE
        LL=L/10+2
        IF(I-3) 1140,1160,1500
1140
        IF(L.EQ.3.OR.L.EQ.13.OR.L.EQ.27) GOTO 1150
        GOTO 1500
1150
        WRITE(5,300) 390+L*10, (VAL(M),M=1,2)
        IF(VAL(2).LT.UL(LL).AND.VAL(2).GT.OW(LL)) GOTO 1500
        WRITE(5,210) 3904L*10,(SPL(M,I),M=1,4)
        GOTO 960
        IF(L.NE.15) GOTO 1500
1160
        IF(VAL(2).LT.UL(5).AND.VAL(2).GT.DU(5)) GOTO 1500
        WRITE(5,210) 540, (SPL(M,3), M=1,4)
        GOTO 960
1500
        CONTINUE
2000
        CONTINUE
C
        I IS THE TRISTIMULUS COUNTER
\mathbb{C}
        J IS THE AVERAGES COUNTER
C
        K IS THE SAMPLE NUMBER OF THE PLASTIC CHIPS COUNTER
        L IS THE WAVELENGTH COUNTER
\mathbf{C}
        DO 2900 I=1.3
        TRIO(1)=0.
        DO 2900 L≈1,32
2900
        TRIO(I)=TRIO(I)+100.*CMF(I,L)*D65(L)
        TH=1./3.
        DO 3050 K#1,2
        DO 3050 J#1.2
        DC 3020 I:1,3
        TR1(],J,K):0.
        10 3000 L=1,32
```

Appendix C (continued)

```
3000
        TRI(I,J,K)=TRI(I,J,K) + RC(L,J,K)*CMF(I,L)*DA5(L)
3020
        TRI(I,J,K)=TRI(I,J,K)/TRIO(I)
3050
        CONTINUE
        DO 3080 I=1,3
        DO 3080 J=1,2
        DU 3080 K=1,2
3080
        HTRI(I,J,K)=TRI(I,J,K)**TH
        DO 3150 K=1,2
        DO 3150 J≈1,2
        STAR(1,J,K)=116.0*TRI(2,J,K)-16.0
        STAR(2)J_{V}K)=500**(TRI(1)J_{V}K)-TRI(2)J_{V}K)
3150
        STAR(3,J,K)=200.*(TRI(2,J,K)-TRI(3,J,K))
        J=:2
        DO 3200 I=1,3
3200
        STAR(I,J,1)=(STAR(I,J,2)-STAR(I,J,1))*(STAR(I,J,2)-STAR(I,J,1))
        CD(1,J)=SQRT(STAR(1,J,1))
        CD(2,J)=SQRT(STAR(2,J,1)*STAR(2,J,1) + STAR(3,J,1)*STAR(3,J,1))
        CD(3,J)=SQRT(CD(1,J)*CD(1,J) + CD(2,J)*CD(2,J))
        WRITE(5,700) (CD(M,J),M=1,3)
        IF(CD(3,2).LT.UL(6).AMD.CD(3,2).GT.OW(6)) GOT04000
        WRITE(5,220)
        NSAM#4
        60TO 950
4000
        STOP
        END
```

Appendix D

Computer program QSTANH for standardization program of Hunter D54.

```
PROGRAM QSTANH
        ---TO PROVIDE A STANDARDIZATION PROCEDURE
       APPLICABLE TO THE HUNTER D54P SPECTROPHOTOMFTER
       DIMENSION AV(6), AVGNO(4), CD(3, 13), CMF(3, 32), D65(32)
       DIMENSION WATER), AND (BZ), PLASI(Z)
        11/16/131 ni hi 32,101, nc (32, i 3, 2), no (32), 3PL (4, n), 31(0)
       DIMERSION STAR(3,13,2),TRI(3,13,2),TRIO(3), VAL(3)
       DATA_CHEZO.0191,0.0020,0.0860,0.0847,0.0088,0.3894
     ~. 0. 2045.0. 0214.0. 9725.0. 3147.0. 0387. 1. 5535
     -, 0.3337, 0.0521, 1.9673, 0.3707, 0.0895, 1.9948
     -,0.3023,0,1282,1.7454,0.1956,0.1852,1.3176
     -, 0.0805, 0.2535, 0.7721, 0.0162, 0.3391, 0.4153
     ~,0.0038,0.4608,0.2185,0.0375,0.6067,0.1120
     -,0.1177,0.7618,0.9607,0.2365,0.8752,0.9395
     ~,7.3768,0.9629,9.0137,0.5298,0.9918,0.0040
     -,).7052,0.9973,0.0000,0.8787,0.9556,0.0000
     -,1,0142,0,8689,0,0000,1,1185,0,7774,0,0000
     -,1.1240,0.6583,0.0000,1.0305,0.5280,0.000
     -, 7.8563, 9.3981, 0.0000, 9.6475, 0.2835, 0.0000
     -,0.4316,0.1793,0.0000,0.2683,0.1076,0.0000
     -,0.1526,0.0603,0.0000,0.0813,0.0318,0.0000
     -. 0.0409.0.0159.0.0000.0.0199.0.0077.0.0000
     -,>.>>>6,0,0037,0.0000,0.0046,0.0018,0.0000/
       DATA D65/828.,916.,935.,868.,1049.,1171.,1178.,1149.,1159.,1083.,
     -1094.,1078.,1049.,1077.,1044.,1040.,1000.,964.,957.,886.,
     -900.,896.,876.,833.,837.,800.,802.,822.,783.,697.,716.,743./
       DATA SPL/AMBE. R FI. LTER. WHIT. E TI. LE GRAY. POR. CELA. IN
                 /STD /,/TAN /,/PLAS/,/TIC /,
                 'SPL ', 'TAN ', 'PLAS', 'TIC '/
       TETA AVGNO, PLAST/ ONE . . AV2 . . AV10 . . SIG . . STD . . SPL //
   -1=AMBER-1420;?=AMBER-0520;3=AMBER-060;4=OPAL-0540;5=GRAY-0540;6=COU. DIFF.
       DATA ST/3.48,38.68,80.20,98.36,42.96,1.88/
       DATA AV/0.03,0.18,0.12,0.10,0.10,0.05/
       DATA NM1/420,520,660,540,540/
       FORMAT(/ DATE: 1.12.2(//1.12))
FORMAT(// 1. ON 054 PRESS MASCH OUTM. THEN MOM. THEN MIRATEMA/
1.00
120
             PUT WHITE PORCELAIN OVER PORT. */
             BLOCK BEAM WITH BLACK CARDBOARD //
        2. PRESS "ZERO". REMOVE CARDBOARDY/
     -/ 3. PRESS "STDZ". AFTER "STANDARDIZED" PRINTS OUT ON D54//
     -/ 4. PRESS "ASCII", THEN "2".//
     -/ 5. PRESS "RETURN" OR SPC-16 CORSOLE PRINTER()
       FORMAT( / BEGIN WITH SAMPLE NO.? (1-5)/)
150
170
       三)?'fAT(ノノ*** REMOVE A''GER FILTER****//
     -/ 1. ON D54, PRESS "ASCII", THEN "O", THEN "R-SIN"//
             PUT ZERO TRAP OVER PORTY
     -/ 2. PRESS "ZERO". PUT WHITE PORCELAIN OVER PORT!/
     -/ 3. PRESS "STDZ". PUT GRAY PORCELAIN OVER PORT!
     -/ !. PRESS "STDZ". AFTER "STANDARDIZED" PRINTS OUT ON D54,//
     -/ o. PRESS "ASCH". THEE "2"//
     -/ A. PRESS "RUTURN" ON SPC-16 CONSOLE PRINTURY)
200
       TORMAT(// MEASURE: /4A4/ INSERT SAMPLE IN D54://
```

Appendix D (continued)

```
AFTER A PAUSE IS PRINTED, PRESS "READ" ON 054//
AFTER BELL RINGS, PRESS "10NM" AND "RETURN" AT SAME TIME()
210
        FORMAT(//****READING AT/15/HW IS OUT OF SPECS FOR*/4A4/
        WASH SAMPLE, THEM!)
FURMALL ALT, 14, ON UPPER LIMIT, F6.2, LOWER LIMIT, F6.2)
2/11
200
        POALMATO COLOR DIFFERENCE: UPPER LIMITYF6.27 LOWER [IMITYF6.2]
240
         TRMAT(//*** COLOR DIFFERENCE IS OUT OF SPECS FOR: /.4A4/
            WASH TILES, THEN!)
        FORMAT(V)
250
300
        FORMT(15,3F10.2,F10.3)
        FORMAT(I3,FII.2)
350
        FOR'MAT(/2(2XA4), / X=/,F7.5, / Y=/,F7.5, / Z=/,F7.5)
450
        FORMAT( / N/L1,5X, /FIRST/, 4X, /AVG OF 21)
500
        FOR'SAT(/A4, / DL=/,F7.2, / DC=/,F7.2, / DE=/,F7.2)
700
800
        FORMAT(///***OK TO MAKE MEASUREMENTS***/)
        CALL FREMAT
        CALL DATESB(IY, IM, ID)
        WRITE(5,100) IM, ID, IY
        WRITE(5,150)
        READ(5,250) MSAH
        IF ("SA".GT.1) GOTO 950
        #RITE(5,120)
        PAUSE
950
        00 2000 II=1.5
        IF(II.LT.NSAM) GOTO 2000
960
        I = II
        IF(I.NE.2) GOTO 970
        WRITE(5,170)
        PAUSE
970
        47ITF(5,200) (SPL(M.I).M=1.4)
        K = 1
        IF(I.NF.1) K=I+2
        1F(I.EQ.5) GOTO 978
        UL=ST(K)+AV(K)
975
        O =ST(K)-AV(K)
        IF(I.EO.4) WRITE(5,230) UL,OW
        IF(I.E0.4) GOTO 978
        署31丁月(5,220) 刊刊(K),UL,OW
        IF(I.NE.1) GOTO 978
        IF(K.EQ.3) GOTO 978
        K=K+1
       GOTO 975
978
       CONTINUE
       DO 1000 N=1.2
       PAUSE
       DO 980 L=1,32
       R(U,V) = RG(U)
       READ(14,350) NWL(L),RG(L)
930
       COUTINUE
       100 985 L=1.32
       RG N =RGC)
985
       CONTINUE
1000
```

IF(I.LT.4) WRITE(5,500)

Appendix D (continued)

```
K=1
        IF(I.NF.1) K=I+2
1100
       00 1140 L=1.32
       VAL(2)=0.
       ひひけてい ヤニナ・シ
        IF(".E0.1) VAL(1)=8(L,\forall)
        IF('I.EQ.1.AND.I.GE.4) RC(L,1,I-3)=VAL(1)
        IF(1.LE.2) VAL(2)=R(L.N)*0.5+VAL(2)
        IF(Y.EQ.2.AND.I.GE.4) RC(L.2,I-3)=VAL(2)
1120
       CONTINUE
       IF(I.GE.4) GOTO 1140
       111=390+L*10
       IF(W.NE. WYI(K)) GOTO 1140
       WRITE(5,300) NY, (VAL(M), M=1,2)
       IF (ABS(VAL(2)-ST(K)).LT.AV(K)) GOTO 1135
       MRITE(5,210) NM((K),(SPL(M,I),M=1,4)
       GOTO 970
1135
       IF(I.EO.1.AND.K.LT.3) K=K+1
1140
       CONTINUE
2000
       CONTINUE
C
       I IS THE TRISTIMULUS COUNTER
C
       J IS THE AVERAGES COUNTER
C
       K IS THE SAMPLE NUMBER OF THE PLASTIC CHIPS COUNTER
C
         IS THE WAVELENGTH COUNTER
       DO 2900 I=1.3
       TRIO(I)=0.
       00 2900 L=1,32
2900
       TRID(I)=TRIO(I)+100.*C!(F(I,L)*D65(L).
       TH=1./3.
       DO 3070 K=1,2
       20 3270 J=1,2
       DO 3020 I=1.3
       TRI(I,J,E)=0.
       100 3000 L=1.32
       TRI(I,J,K)=TRI(I,J,K)+RC(L,J,K)+CMF(I,L)*D65(L)
       COUTINUE
3000
       TRICL, J, K)=TRICL, J, K)/TRICCL)
3020
       WRITE(5,450) PLAST(K), AVGNO(J), (TRI(M, J, K), M=1,3)
C
3070
       CONTINUE
       "):) 3080 T=1,3
       no 3080 J=1.2
       00 3080 K=1.2
       \Gamma RI(I,J,K) = \Gamma RI(I,J,K) **TH
3080
       )) 3170 K=1.2
)) 3170 J=1.2
       SEMI(1,J,E)=116.0%TRI(2,J,E)-16.0
       STAR(2,J,K)=500.*(TRI(1,J,K)~TRI(2,J,K))
       $EVR(3,1,K)=200.*(FRI(2,J,K)~TRI(3,J,K))
3170
       CONTINUE
       99 7250 J=1,2
3120
        30 3200 1=1.3
3200
        $ENRCL,J,L)=CSTARCL,J,2)-SFARCL,J,L))*(STARCL,J,2)-STARCL,J,L)^
       CY(1,J) = JORR(STAR(1,J,1))
       COCT, J) = 500T (STARCP, J, 1) *STARCP, J, 1) + STARC3, J, 1) *STARC3, J, 1)
```

Appendix D (continued)